August 1, 2023

Jesse Winterowd
Winterbrook Planning
610 SW Alder Street, Suite 810
Portland, OR 97205

Subject: Supplemental Information
Re: Land Use Permitting

## Dear Jesse:

Delve Underground was asked to provide additional information in regard to the "expansive soil" and "Fat Clay" layer identified in in response to comments on those issues included in a memorandum prepared by True North Geotechnical dated June 28, 2023 (Exhibit E.21). An extensive geotechnical exploration program was performed on the project site, all relevant soil layers were identified with recommendations for design and construction provided to the Portland Water Bureau and design team.

Expansive soils are clayey soils, generally Fat Clays containing specific clay minerals, that exhibit volume changes due to changes in water content. Fat Clay was not encountered in the explorations near the proposed shaft location. Fat Clay soils were identified in field explorations in eastern half of the raw water pipeline (RWP) alignment, within the upper 20 feet of the ground. Attached are the project site plan showing the exploration locations and logs of the borings completed by Delve Underground. Borings in which fat clay was identified are highlighted in green. The pipeline in this section of the alignment will be embedded in gravelly soils, below fat clay. Gravelly soils are not susceptible to expansion. The foundations of ancillary structures such as manholes or access way structures will also be constructed on gravelly soils. Therefore, presence of fat clay in this section of the alignment is not anticipated to impact the pipeline and associated structures.

The map of expansive soils in the U.S. by Olive, et al. (1989) identifies soils within eastern part of the Portland metro as "Little or no Swelling Clay". Specific testing of the expansive potential of the Fat Clays was not performed because the design of the pipeline is not sensitive to the expansive properties on account of the pipeline being founded on material below the Fat Clay and because steel pipes, which will be utilized in this project, are flexible elements that can accommodate a moderate amount of deformation.

Supplemental Information
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The conclusion provided in Exhibit A. 82 that "Based on a review of published geologic and seismic hazard mapping and the explorations and analyses performed for the project as documented in this report, the location of the RWP section of the Pipelines project is suitable for the proposed development", remains valid.

Sincerely,
Harar saramier
Fard Sariosseiri, PE
Lead Associate
cc: File


MOISTURE CONTENT

| DESCRIPTION | CONDITION |
| :---: | :--- |
| Dry | Absence of moisture, dusty, dry to the touch. |
| Moist | Damp, but no visible water. |
| Wet | Visible free water, typically below water table. |

ABBREVIATIONS

| SYMBOL | DEFINITION |
| :---: | :---: |
| $H$ | Atterberg Limits |
| $\bigcirc$ | Moisture Content |
| $\square$ | Blows per foot ( N ) |

COARSE-GRAINED SOIL DENSITY

| Relative Density | N, SPT <br> Blows/foot |
| :---: | :---: |
| Very Loose | 0 to 4 |
| Loose | 5 to 10 |
| Medium Dense | 11 to 30 |
| Dense | 31 to 50 |
| Very Dense | $>50$ |

PERCENTAGE RANGE TERMS ${ }^{1,2}$

| DESCRIPTION | RANGE |
| :---: | :---: |
| Trace | $<5 \%$ |
| Few | 5 to $10 \%$ |
| Little | 15 to $25 \%$ |
| Some | 30 to $45 \%$ |
| Mostly |  |
| 50 to $100 \%$ |  |
| 1. Gravel, Sand and fines are estimated <br> by mass. Other constituents such as <br> organics, cobbles, and boulders are <br> estimated by volume. |  |
| 2. Percentages per ASTM D2488. |  |

PARTICLE SIZE DEFINITIONS

| DESCRIPTON |  | SIEVE SIZE PER ASTM D2488 |
| :---: | :---: | :---: |
| FINES |  | <\#200 (0.075 mm) |
| SAND | Fine | \#200 to \#40 (0.075 to 0.4 mm ) |
|  | Medium | \#40 to \#10 ( 0.4 to 2 mm ) |
|  | Coarse | \#10 to \#4 (0.4 to 4.75 mm ) |
| GRAVEL | Fine | \#4 to $3 / 4 \mathrm{in}$. (4.75 to 19 mm ) |
|  | Medium | $3 / 4$ to 3 in. (19 to 76 mm ) |
| COBBLES |  | 3 to 12 in . (76 to 305 mm ) |
| BOULDERS |  | > 12 in. ( 305 mm ) |


| UNIFIED SOIL CLASSIFICATION SYSTEM（USCS）${ }^{1}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MAJOR DIVISIONS |  |  |  | SYMBOL |  | TYPICAL DESCRIPTION | ALTERNATE DESCRIPTIONS |
|  |  | CLEAN GRAVELS <br> （ $\leq 5 \%$ FINES） |  | GW |  | WELL－GRADED GRAVEL | WELL－GRADED GRAVEL WITH SAND |
|  |  |  |  | GP | \| | POORLY GRADED GRAVEL | POORLY GRADED GRAVEL WITH SAND |
|  |  | GRAVELS ${ }^{2,4}$ <br> （ $5-12 \%$ FINES） |  | GW－GM |  | WELL－GRADED GRAVEL WITH SILT | WELL－GRADED GRAVEL WITH SILT AND SAND |
|  |  |  |  | GW－GC |  | WELL－GRADED GRAVEL WITH CLAY | WELL－GRADED GRAVEL WITH CLAY AND SAND |
|  |  |  |  | GP－GM |  | POORLY GRADED GRAVEL WITH SILT | POORLY GRADED GRAVEL WITH SILT AND SAND |
|  |  |  |  | GP－GC |  | POORLY GRADED GRAVEL WITH CLAY | POORLY GRADED GRAVEL WITH CLAY AND SAND |
|  |  | $\begin{aligned} & \text { GRAVELS WITH } \\ & \text { FINES } \\ & (\geq 12 \% \text { FINES) } \\ & \hline \end{aligned}$ |  | GM |  | SILTY GRAVEL | SILTY GRAVEL WITH SAND |
|  |  |  |  | GC |  | CLAYEY GRAVEL | CLAYEY GRAVEL WITH SAND |
|  |  | CLEAN SANDS （ $\leq 5 \%$ FINES） |  | SW |  | WELL－GRADED SAND | WELL－GRADED SAND WITH GRAVEL |
|  |  |  |  | SP | ．．． | POORLY GRADED SAND | POORLY GRADED SAND WITH GRAVEL |
|  |  | $\begin{gathered} \text { SANDS }{ }^{2,4} \\ (5-12 \% \text { FINES }) \end{gathered}$ |  | SW－SM | Eve | WELL－GRADED SAND WITH SILT | WELL－GRADED SAND WITH SILT AND GRAVEL |
|  |  |  |  | SW－SC |  | WELL－GRADED SAND WITH CLAY | WELL－GRADED SAND WITH CLAY AND GRAVEL |
|  |  |  |  | SP－SM | 㸱淮家 | POORLY GRADED SAND WITH SILT | POORLY GRADED SAND WITH SILT AND GRAVEL |
|  |  |  |  | SP－SC |  | POORLY GRADED SAND WITH CLAY | POORLY GRADED SAND WITH CLAY AND GRAVEL |
|  |  | $\begin{aligned} & \hline \text { SANDS WITH } \\ & \text { FINES }^{3} \\ & (>12 \% \text { FINES }) \\ & \hline \end{aligned}$ |  | SM |  | SILTY SAND | SILTY SAND WITH GRAVEL |
|  |  |  |  | SC | 䒴湾 | CLAYEY SAND | CLAYEY SAND WITH GRAVEL |
|  | SILTS AND <br> CLAYS <br> （LL＜50） |  | INORGANIC | ML | ｜｜｜｜｜｜｜ | SILT | SILT WITH SAND OR GRAVEL； SANDY OR GRAVELLY SILT |
|  |  |  | CL |  | LEAN CLAY | LEAN CLĀ $\mathbf{~ W I T H M ~ S A A N D ~ O R ~ G R A V E L ; ~}$ SANDY OR GRAVELLY LEAN CLAY |
|  |  |  | ORGANIC | OL | $\begin{array}{\|l\|} \hline \text { "दर } \\ \hline \end{array}$ | ORGANIC SOIL | ORGANIC SOIL WITH SAND OR GRAVEL； SANDY OR GRAVELLY ORGANIC SOIL |
|  | SILTS AND |  |  | INORGANIC | MH | \｜W\｜ | ELASTIC SILT | ELASTIC SILT WITH SAND OR GRAVEL； SANDY OR GRAVELLY ELASTIC SILT |
|  | CLAYS$(L L \geq 50)$ |  | CH |  |  | FAT CLAY | FAT CLĀ Y WITH SAND OOR GRAVEL； SANDY OR GRAVELLY FAT CLAY |
|  |  |  | ORGANIC | OH | \}? ${ }^{\text {m }}$ | ORGANIC SOIL | ORGANIC SOIL WITH SAND OR GRAVEL； SANDY OR GRAVELLY ORGANIC SOIL |
|  | SILT／CL |  | INORGANIC | CL－ML | ｜TV／A | SILTY CLAY | SILTY CLAY WITH SAND OR GRAVEL； SANDY OR GRAVELLY SILTY CLAY |
| HIGHLY ORGANIC SOILS |  |  | ORGANIC | PT | 4－24 | PEAT |  |

## NOTES：

1．The USCS described here is based on ASTM standards D2487 \＆D2488．
2．Dual symbol materials（e．g．，SP－SM）are used for soils between $5 \%$ and $12 \%$ fines or when liquid limit and plasticity index values plot in the CL－ML area of the plasticity chart，（LL：12－25，PI：4－7）．
3．ASTM D2488 specifies the use of dual symbol coarse－grained soils between $5 \%$ and $15 \%$ fines．

| BACKFILL，WELL，AND SAMPLE SYMBOLS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 韭曲 | Bentonite Chips | Div | Grout | 又 | 2＂OD Split Barrel Sampler |
| \％ | Concrete | $\square$ | Observation Well－Solid | $\square$ | Shelby Tube Sample |
|  | Sand | 青 | Observation Well－Screen | 240 | Grab Sample |
|  | Asphalt | ［｜ | Vibrating Wire Piezometer | ［ | Rock Core Run |
| $\because$ | Gravel | 三 | Measured Groundwater Level |  |  |

## Key to Rock Core Logs

| Rock Strength |  |  |  |
| :---: | :---: | :---: | :---: |
| Grade $^{1}$ | Description | Recognition | UCS $^{2}$ (psi) |
| R0 | Extremely Weak | Indented by thumbnail | 30 to 150 |
| R1 | Very Weak | Peeled by pocketknife | 150 to 700 |
| R2 | Weak | Peeled with difficulty by <br> pocketknife | 700 to 3,600 |
| R3 | Medium Strong | Indented 5 mm with <br> sharp end of pick | 3,600 to 7,200 |
| R4 | Strong | One hammer blow to <br> fracture | 7,200 to 14,500 |
| R5 | Very Strong | Many hammer blows to <br> fracture | 14,500 to 36,000 |
| R6 | Extremely Strong | Only chipped by hammer <br> blows | $>36,000$ |
| 1: Rock strength grades from Brown (1981) <br> 2: Uniaxial Compressive Strength (pounds per square inch) |  |  |  |

## Rock Weathering/Alteration

| Residual Soil | Entirely decomposed to secondary minerals; material <br> can be easily broken by hand |
| :---: | :---: |
| Completely <br> Weathered/Altered | Almost entirely decomposed to secondary minerals; <br> material can be granulated by hand |
| Highly Weathered/Altered | More than half of the rock is decomposed |
| Moderately <br> Weathered/Altered | Rock is discolored and noticeably weakened, but less <br> than half is decomposed |
| Slightly <br> Weathered/Altered | Rock is slightly discolored, but not noticeably lower in <br> strength than fresh rock |
| Fresh/Unweathered | Rock shows no discoloration, loss of strength, or other <br> effect of weathering or alteration |

Rock Fracture Spacing

| IF | Intensely Fractured | Fractures spaced less than 2 inches apart |
| :---: | :---: | :---: |
| HF | Highly Fractured | Fractures spaced 2 inches to 1 foot apart |
| MF | Moderately Fractured | Fractures spaced 1 foot to 3 feet apart |
| SF | Slightly Fractured | Fractures spaced 3 feet to 10 feet apart |
| M | Massive | Fracture spacing greater than 10 feet |

Lithology Graphics


Core Recovery Calculation (\%)

| $\frac{\Sigma \text { Length of the recovered core pieces }}{\text { Total Length of core run }} \times 100$ |
| :---: |
| RQD Calculation (\%) |
| $\frac{\Sigma \text { Length of intact core pieces }>4 \text { in. }}{\text { Total Length of core run }} \times 100$ |


| Discontinuity Type |  |
| :---: | :---: |
| J | Joint |
| MB | Mechanical Break |
| FJ | Joint along foliation |
| S | Shear |
| F | Fault |
| HJ | Healed joint |
| B | Joint along bedding |


| Shape | Aperture (Inches) |  |
| :---: | :---: | :---: |
|  | VW | Wide (<1.0) |
|  | W | Moderately Wide (0.2-1.0) |
|  | N | Narrow (0.05-0.2) |
|  | VN | Very Narrow (0-0.05) |
|  | T | Tight (0) |


| Curved (C) | Surface Roughness |  |
| :---: | :---: | :---: |
| SLK | Slickensided |  |
| Undulating (U) | Smooth |  |
| SR | Slightly Rough |  |
| R | Rough |  |
| VR | Very Rough |  |

Bedding Spacing

| Very Thin | Laminated (<2 <br> in.) |
| :---: | :---: |
| Thin | 2 in to 1 ft |
| Medium | 1 ft to 3 ft |
| Thick | 3 ft to 10 ft |
| Very <br> Thick | $>10 \mathrm{ft}$ |

Joint Infill

| CL | Clay | Ctg | Coating/ <br> Staining | Fe | Iron Oxide | U Unknown |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fi | $100 \%$ Filling | -- | None/ <br> Not observed | Si | Silt |  |  |

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Log of Boring
LRWP-BH05


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Log of Boring
LRWP-BH05


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Log of Boring
LRWP-BH05


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Project: Filtration Pipelines Project - Raw Water Pipeline
Project Location: Multnomah County, OR
Project Number: 6218.0


NOTES:
Location and Elevation Source: 90\% Drawings
Vertical Datum: Portland Vertical Datum Feet (NAVD88-2.1)
Coordinate System: Water Bureau Filtration Project Custom Coordinate System

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LRWP-BH06


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LRWP-BH07


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Project Number: 6218.0

| Date(s) <br> Drilled | 11/16/2021 - 11/30/2021 | Client | Jacobs Engineering Group |
| :--- | :--- | :--- | :--- | :--- | :--- | | Final |
| :--- |
| Depth |$\quad$ 232.0 ft bgs | 230 |
| :--- |

Project: Filtration Pipelines Project - Raw Water Pipeline
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Log of Boring
LRWP-BH07

| Date(s) Drilled | 11/16/2021-11/30/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l\|} \hline \text { Final } \\ \text { Depth } \\ \hline \end{array}$ | 232.0 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742874.8 E, 659436.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary and HQ Wireline/CME 850 Track Mounted |
| Surface Elevation | 707.5 ft . | $\begin{array}{\|l\|} \hline \text { Drilling } \\ \text { Contractor } \end{array}$ | Western States Soil Conservation, Inc. | Hole Diameter | 4.00 in |
| Location | LRWP North Station 29+98 | Logged by/ Checked by | K. Elliott, A. Judy / K. Elliott | Hammer Tyne | 140 lb / 30 in / Automatic |

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| :--- | :--- | :--- | :--- | :--- | :--- | | Final |
| :--- |
| Depth |$\quad$ 232.0 ft bgs | 230 |
| :--- |



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| $\begin{aligned} & \text { Date(s) } \\ & \text { Drilled } \end{aligned}$ | 11/16/2021-11/30/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l\|} \hline \text { Final } \\ \text { Depth } \end{array}$ | 232.0 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | $7742874.8 \mathrm{E}, 659436.9 \mathrm{~N}$ | Geotechnical Consultant | McMillen Jacobs Associates | Method/ | Mud Rotary and HQ Wireline/CME 850 Track Mounted |
| Surface <br> Elevation | 707.5 ft . | Dilling Contractor | Western States Soil Conservation, Inc. | Hole Diameter | 4.00 in |
| Location | LRWP North Station 29+98 | Logged byl <br> Checked by | K. Elliott, A. Judy / K. Elliott | Hammer Type | $140 \mathrm{lb} / 30$ in / Automatic |

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| Date(s) Drilled | 11/16/2021-11/30/2021 | Client | Jacobs Engineering Group | $\begin{aligned} & \text { Final } \\ & \text { Depth } \end{aligned}$ | 232.0 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742874.8 E, 659436.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary and HQ Wireline/CME 850 Track Mounted |
| Surface Elevation | 707.5 ft . | Drilling Contractor | Western States Soil Conservation, Inc. | Hole Diameter | 4.00 in |
| Location | LRWP North Station 29+98 | Logged by/ Checked by | K. Elliott, A. Judy / K. Elliott | Hammer Tvine | $140 \mathrm{lb} / 30$ in / Automatic |



NOTES:
Location and Elevation Source: 90\% Drawings
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LRWP-BH07

| Date(s) Drilled | 11/16/2021-11/30/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l} \hline \begin{array}{l} \text { Final } \\ \text { Depth } \end{array} \\ \hline \end{array}$ | 232.0 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742874.8 E, 659436.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary and HQ Wireline/CME 850 Track Mounted |
| Surface Elevation | 707.5 ft . | Drilling Contractor | Western States Soil Conservation, Inc. | $\begin{aligned} & \hline \begin{array}{l} \text { Hole } \\ \text { Diameter } \end{array} \\ & \hline \end{aligned}$ | 4.00 in |
| Location | LRWP North Station 29+98 | Logged byl Checked by | K. Elliott, A. Judy / K. Elliott | Hammer Type | $140 \mathrm{lb} / 30 \mathrm{in}$ / Automatic |



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Log of Boring
LRWP-BH08


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| Date(s) Drilled | 12/02/2021-12/16/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|} \text { Final } \\ \text { Depth } \end{array}$ | 251.6 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742647.7 E, 659429.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary/CME 850 Track Mounted |
| Surface Elevation | 715.2 ft . | Drilling Contractor | Western States Soil Conservation, Inc. | Hole Diameter | 5.00 in |
| Location | LRWP North Station 32+26 | Logged byl Checked by | A. Judy, K. Elliott / K. Elliott, J. Fissel | Hammer Type | $140 \mathrm{lb} / 30 \mathrm{in}$ / Automatic |



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| $\begin{aligned} & \text { Date(s) } \\ & \text { Drilled } \\ & \hline \end{aligned}$ | 12/02/2021-12/16/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l\|} \hline \text { Final } \\ \text { Depth } \end{array}$ | 251.6 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742647.7 E, 659429.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary/CME 850 Track Mounted |
| Surface Elevation | 715.2 ft . | Drilling Contractor | Western States Soil Conservation, Inc. | Hole Diameter | 5.00 in |
| Location | LRWP North Station 32+26 | Logged by/ Checked by | A. Judy, K. Elliott / K. Elliott, J. Fissel | Hammer Type | $140 \mathrm{lb} / 30 \mathrm{in}$ / Automatic |



Project: Filtration Pipelines Project - Raw Water Pipeline
Project Location: Multnomah County, OR
Project Number: 6218.0

| Date(s) Drilled | 12/02/2021-12/16/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l} \text { Final } \\ \text { Depth } \end{array}$ | 251.6 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
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Project: Filtration Pipelines Project - Raw Water Pipeline
Project Location: Multnomah County, OR
Project Number: 6218.0
Log of Boring
LRWP-BH08

| Date(s) Drilled | 12/02/2021-12/16/2021 | Client | Jacobs Engineering Group | $\begin{array}{\|l\|} \hline \text { Final } \\ \text { Depth } \end{array}$ | 251.6 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742647.7 E, 659429.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary/CME 850 Track Mounted |
| Surface Elevation | 715.2 ft . | Drilling Contractor | Western States Soil Conservation, Inc. | Hole Diameter | 5.00 in |
| Location | LRWP North Station 32+26 | Logged byl Checked by | A. Judy, K. Elliott / K. Elliott, J. Fissel | Hammer Type | $140 \mathrm{lb} / 30 \mathrm{in}$ / Automatic |

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Log of Boring
LRWP-BH08

| Date(s) <br> Drilled | 12/02/2021-12/16/2021 | Client | Jacobs Engineering Group | Final Depth | 251.6 ft bgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Coordinates | 7742647.7 E, 659429.9 N | Geotechnical Consultant | McMillen Jacobs Associates | Method/ Riq Type | Mud Rotary/CME 850 Track Mounted |
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| Location | LRWP North Station 32+26 | Logged by/ Checked by | A. Judy, K. Elliott / K. Elliott, J. Fissel | Hammer Type | $140 \mathrm{lb} / 30 \mathrm{in} /$ Automatic |



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