Multnomah County Courthouse Relocation

Portland, Oregon

Transportation Alternatives Analysis Technical Memorandum:

Prepared for

Multnomah County
Facilities and Property Management Division
401 N Dixon
Portland, OR 97227

Prepared by

David Evans and Associates, Inc. 2100 SW River Parkway Portland, Oregon 97201

April 2015

Table of Contents

| 1. | PURPOSE AND STUDY AREA | 1 |
|-----|--------------------------------------|------|
| 2. | FINDINGS | 1 |
| 3. | ANALYSIS ALTERNATIVES | 2 |
| 4. | TRANSPORTATION ANALYSIS OVERVIEW | 2 |
| 5. | OPENING YEAR 2020 TRAFFIC OPERATIONS | 5 |
| 6. | PARKING CONSIDERATIONS | 6 |
| 7. | PEDESTRIAN CONSIDERATIONS | 7 |
| 8. | BICYCLE CONSIDERATIONS | 8 |
| 9. | TRANSIT CONSIDERATIONS | 9 |
| 10. | SITE ACCESS CONSIDERATIONS | . 10 |
| 11. | FREIGHT LOADING CONSIDERATIONS | 10 |
| 12. | TEMPORARY CONSTRUCTION IMPACTS | 10 |
| 13. | CONCLUSIONS | 12 |
| | | |

Appendices

Appendix A: Existing Traffic Counts

Appendix B: Traffic Volumes Development

Appendix C: Synchro Operational Analysis Output

List of Figures

| | Follows page |
|---|---------------------|
| FIGURE 1: STUDY AREA | 1 |
| FIGURE 2: EXISTING (2012) AM & PM PEAK HOUR VOLUMES | 3 |
| FIGURE 3: OPENING YEAR (2015) AM & PM PEAK HOUR VOLUMES WITHOUT A WESTBOUND LEF | TS AT |
| Madison | 3 |
| FIGURE 4: OPENING YEAR (2020) TRAFFIC OPERATIONS PM PEAK HOUR | 6 |
| FIGURE 5: AVAILABLE PARKING | 6 |
| List of Tables | |
| TADLE 1. LEVEL OF SERVICE CRITERIA | 1 |

This page intentionally left blank.

1. PURPOSE AND STUDY AREA

Multnomah County is working to identify a location for a new county central courthouse. The existing courthouse is located in downtown Portland at 1021 Southwest 4th Avenue. As part of the selection process to identify a preferred location for the new courthouse, Multnomah County has identified two potential locations in downtown Portland:

- **Hawthorne Bridgehead Site:** located at the west end of the Hawthorne bridge on the block between SW 1st Avenue and SW Naito Parkway, and SW Madison and SW Jefferson Streets
- Block 128 Site: located on the block between SW 1st and SW 2nd Avenues, and SW Columbia and SW Clay Streets

This memorandum will discuss the traffic analysis completed to evaluate the transportation impacts associated with each site. The analysis included a PM peak hour operations analysis, building access driveway evaluation and determination of implications to pedestrian, transit, and bicycle operations and safety.

In order to capture the impacts of each site, 11 intersections were selected within the area of SW Market Street on the south, SW Madison Street on the north, SW 2nd Avenue on the west, and SW Naito Parkway on the east. The 11 study area intersections are:

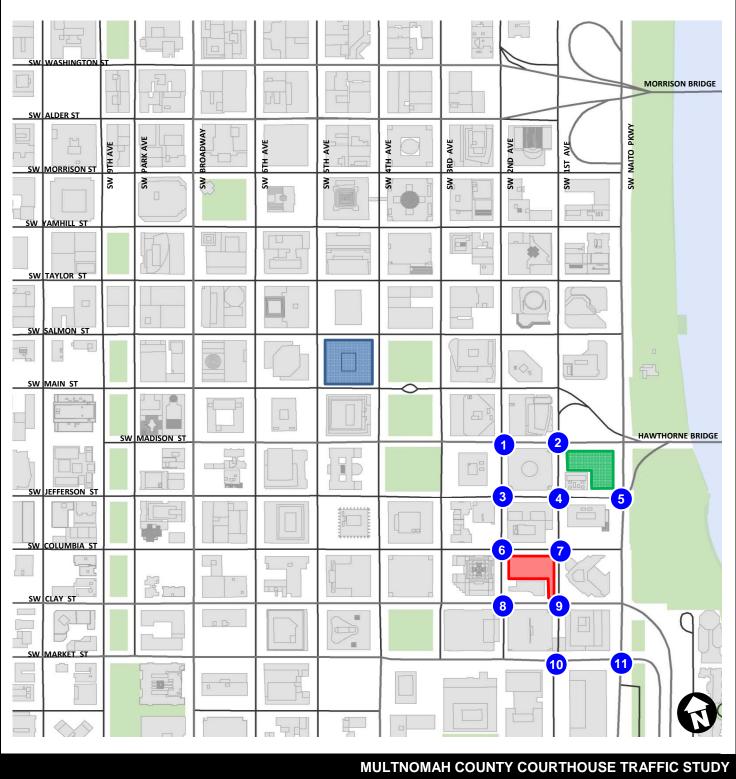
- 1. SW Madison Street at SW 2nd Avenue
- 2. SW Madison Street at SW 1st Avenue
- 3. SW Jefferson Street at SW 2nd Avenue
- 4. SW Jefferson Street at SW 1st Avenue
- SW Jefferson Street at SW Naito Parkway

- 6. SW Columbia Street at SW 2nd Avenue
- 7. SW Columbia Street at SW 1st Avenue
- 8. SW Clay Street at SW 2nd Avenue
- 9. SW Clay Street at SW 1st Avenue
- 10. SW Market Street at SW 1st Avenue
- 11. SW Market Street at SW Naito Parkway

Figure 1 shows the study area and the 11 study area intersections located in downtown Portland.

2. FINDINGS

The results of the transportation analysis indicate that neither the Hawthorne Bridgehead nor Block 128 sites have fatal flaws with respect to transportation. There are unique transportation challenges for each site; however, there are no significant transportation concerns at either location. The overall traffic operations, bicycle, pedestrian, transit, and parking considerations for each site are comparable and do not preclude either site from consideration.



Legend # Intersection Number Hawthorne Bridgehead Site Block 128 Site Existing Courthouse Note: Shape depicts block location only and does not represent the footprint of the proposed courthouse

3. ANALYSIS ALTERNATIVES

Multnomah County has identified two potential locations in downtown Portland where the new county central courthouse could be sited. Each location is described in further detail below.

Hawthorne Bridgehead

The Hawthorne Bridgehead site is enclosed by SW Madison Street on the north, SW Jefferson Street on the south, SW 1st Avenue on the west, and SW Naito Parkway on the east. The site is accessible by all means of transportation including pedestrian, bicycle, auto, bus, and MAX. Traffic circulation around this site would be unchanged from what it is today. This site would have access to an existing garage near the site for public parking and possible secure judge parking. The new courthouse will provide a Sally Port for secure prisoner transfers, with vehicles entering from southbound SW Naito Parkway and exiting onto SW Jefferson Street.

Block 128

The Block 128 site is enclosed by SW Columbia Street on the north, SW Clay Street on the south, SW 2nd Avenue on the west, and SW 1st Avenue on the east. The site is accessible by all means of transportation including pedestrian, bicycle, auto, bus, and MAX. Traffic circulation around this site would be unchanged from what it is today. This site would have access to an existing garage near the site for public parking. The new courthouse will provide a Sally Port for secure prisoner transfers, with vehicles entering from southbound SW 2nd Avenue and exiting onto SW Columbia Street.

4. TRANSPORTATION ANALYSIS OVERVIEW

This section provides the methodology and overview of the transportation analysis. The transportation analysis provides a discussion of existing traffic volumes, the opening year traffic estimates, assumptions for the projected opening year volumes, and a summary of traffic operations. The traffic operations analysis for each of the traffic alignments discussed above was performed on an assumed opening year of 2020.

Existing Traffic Volumes

The existing traffic count data included number of vehicles, vehicle classifications, and bicycle and pedestrian volumes. Traffic volume data collected for this project consisted of PM peak hour intersection turn movement counts collected on Thursday, February 26, 2015 from 4:00 to 6:00 PM.

The turning movement counts were examined to determine the common weekday PM peak hours among the intersections based on the hour with the highest total volume of vehicles on the network. The common peak hour for the intersections was determined to be 4:45 to 5:45 PM. While the peak hour at each intersection may or may not correspond with the common peak hour, all individual peak hours overlap with at least a portion of the common

peak hour. **Figure 2** shows the PM peak hour volumes collected. Detailed traffic count data can be seen in **Appendix A**.

Mode Split

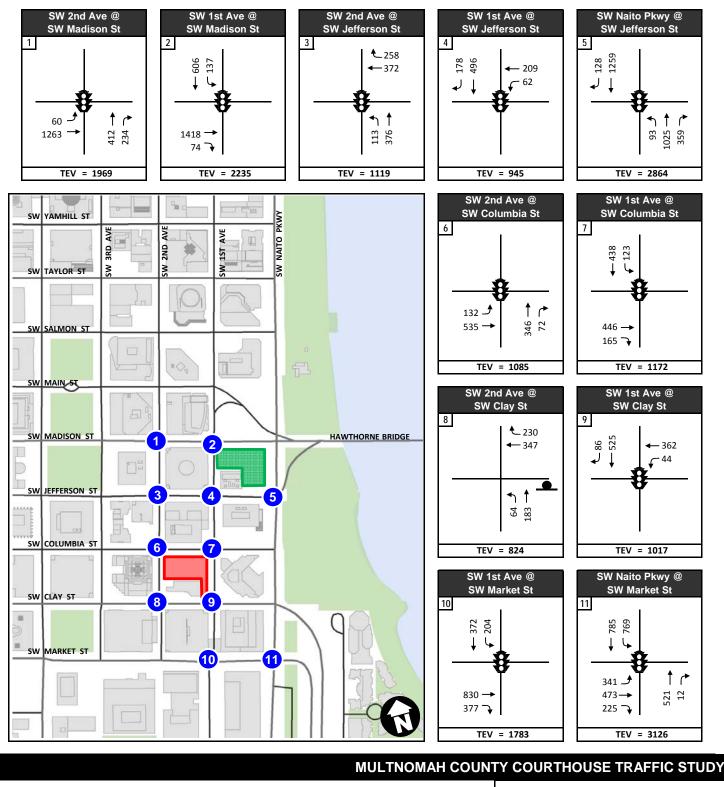
A Central Courthouse Community Survey was conducted by Multnomah County between August 27, 2014 and November 17, 2014. The survey focused on a variety of topics including how users travel to the existing courthouse. The survey found that approximately 38% of all responders travel to the courthouse by motor vehicle (drive or carpool). Twenty-one percent of all responders use transit, four percent bicycle, and 37% walk to the courthouse. Mode split for the new courthouse is not expected to change significantly as a result of relocating the courthouse to either of the proposed sites.

Opening Year Traffic Volumes

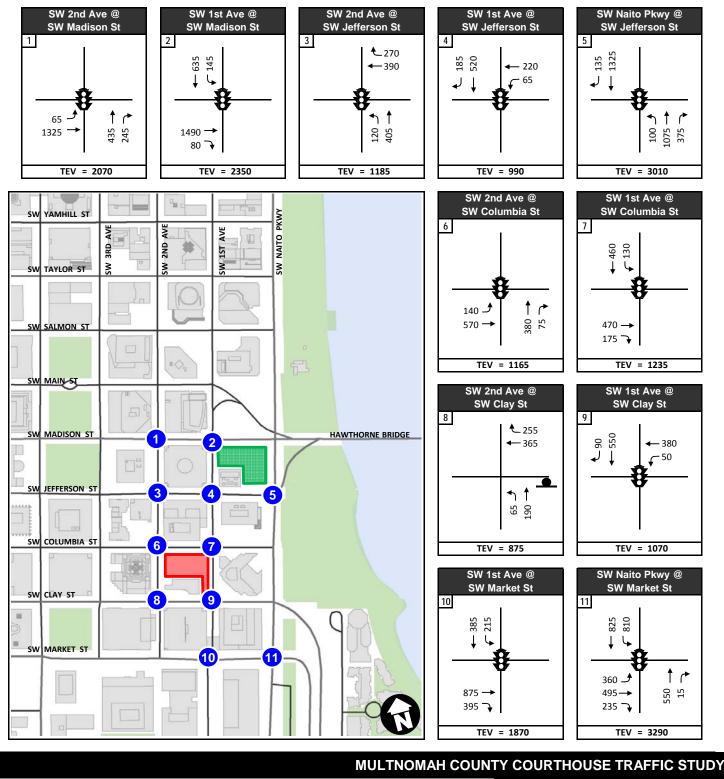
Opening year for the new courthouse was assumed to be 2020. To estimate 2020 traffic volumes, PM peak hour turn movements were projected using a linear growth rate of one percent. **Figure 3** shows the PM peak hour volumes for the opening year of 2020. Calculations used to grow existing 2015 volumes to opening year 2020 volumes can be found in **Appendix B**.

For developing opening year (2020) volumes it was assumed that the relocated courthouse will add no net new vehicular trips to the overall downtown network, eliminating the need for a baseline versus build scenario analysis. The new courthouse is expected to feature similar numbers of employees and courtrooms; however, the new courthouse will not have four (4) high volume courtrooms (parking citations, other violations (primarily traffic citations), Small Claims, and Landlord-Tenant (FED) cases which are major trip generator for the current courthouse. The comparable numbers of employees and courts suggest that the current trips generated by the existing courthouse will simply be diverted to the new location a few blocks southeast of the current site and are not new trips to the downtown network. Furthermore, the lack of high volume courts in the new courthouse indicates that trips generated by the existing traffic courts will not be diverted to the new site at all. The total trips traveling to the new courthouse are not anticipated to exceed the number of existing trips.

For the majority of courthouse employees and visitors traveling to the courthouse from the west side, routes to the two proposed courthouse locations will be mostly unchanged. For employees and visitors traveling from the east side, slight shifts in trips across the Willamette River bridges may be experienced due to the relocation of the courthouse a few blocks to the south. It is assumed general PM peak hour travel patterns to the new sites will reflect typical downtown travel patterns and result in no change in traffic volumes. Travel patterns to the two proposed sites are likely to be very similar due to their close proximity to each other and the existing site. To quantify any potential shifts in traffic patterns and volumes that may occur at either of the proposed sites would require a detailed trip generation study of the existing courthouse.



Legend Turning Movement Signalized Intersection Figure 2 Existing (2015) Conditions PM Peak Hour Traffic Counts H## PM Peak Hour Volume Hawthorne Bridgehead Site Block 128 Site Note: Shape depicts block location only and does not represent the footprint of the proposed courthouse



Legend Turning Movement Signalized Intersection Figure 3 Opening Year (2020) Conditions PM Peak Hour Volumes ### PM Peak Hour Volume Hawthorne Bridgehead Site Block 128 Site Note: Shape depicts block location only and does not represent the footprint of the proposed courthouse

Traffic Operations Overview

Operational Criteria

Transportation engineers have established various methods for measuring traffic operations of roadways and intersections. Most jurisdictions use either volume-to-capacity (v/c) ratio or level of service (LOS) to establish performance criteria. Both the LOS and v/c ratio concepts require consideration of factors that include traffic demand, capacity of the intersection or roadway, delay, frequency of interruptions in traffic flow, relative freedom for traffic maneuvers, driving comfort, convenience, and operating cost.

Volume-to-Capacity (v/c) Ratio

A comparison of traffic volume demand to intersection capacity is one method of evaluating how well an intersection is operating. This comparison is presented as a v/c ratio. A v/c ratio of less than 1.00 indicates that the volume is less than capacity. When the v/c ratio is closer to zero, traffic conditions are generally good, with little congestion and low delays for most intersection movements. As the v/c ratio approaches 1.00, traffic becomes more congested and unstable, with longer delays.

Level of Service (LOS)

LOS is also a widely recognized and accepted measure and descriptor of traffic operations. At both STOP-controlled and signalized intersections, LOS is a function of control delay, which includes initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay. Six standards have been established, ranging from LOS A, where there is little or no delay, to LOS F, where there is delay of more than 50 seconds at unsignalized intersections, or more than 80 seconds at signalized intersections. Table 1 illustrates the level of service criteria for signalized and unsignalized intersections according to the Highway Capacity Manual.

Table 1: Level of Service Criteria

| Level of Service | Average Contro | l Delay (sec/veh) |
|----------------------------|--------------------------|----------------------------|
| | Signalized Intersections | Unsignalized Intersections |
| Α | ≤10 | 0 – 10 |
| В | >10 - 20 | >10 – 15 |
| С | >20 - 35 | >15 – 25 |
| D | >35 - 55 | >25 – 35 |
| E | >55 - 80 | >35 – 50 |
| F | >80 | >50 |
| Source: 2000 Highway Capac | ity Manual | |

It should be noted that, although delays can sometimes be long for some movements at a STOP-controlled intersection, the v/c ratio may indicate that there is adequate capacity to process the demand for that movement. Similarly, at signalized intersections, some

movements, particularly side street approaches or left turns onto side streets, may experience longer delays because they receive only a small portion of the green time during a signal cycle, but their v/c ratio may be relatively low. For these reasons, it is important to examine both v/c ratio and LOS when evaluating overall intersection operations. Both are reported in the following section.

Operational Guidelines

The City of Portland uses a performance guideline based on LOS. The Portland Bureau of Transportation (PBOT) Transportation System Plan (TSP) states that signalized intersections must meet LOS D. Unsignalized intersections are required to operate at LOS E. In addition, the City of Portland has a practice not to reduce the portal capacity into downtown. This means that additional queuing or increased delay that would reduce the number of vehicles entering into downtown would be unacceptable.

Traffic Operations Analysis Procedures

All operations were evaluated using the methodology outlined in the 2000 Highway Capacity Manual (HCM). The Synchro/SimTraffic analysis software was selected for performing the intersection analysis, since it can provide the v/c ratio and LOS output of an HCM analysis as well as consider the systematic interaction of the intersections with regard to queuing and delays.

Synchro is a macroscopic model similar to the Highway Capacity Software (HCS), and like the HCS, is based on the 2000 HCM. The Synchro model explicitly evaluates traffic operations under coordinated and uncoordinated systems of signalized and unsignalized intersections. The v/c ratios and LOS presented in this report are based on the Synchro model output.

Signal Timing

The downtown signal system is currently operating with a 60-second cycle length during the PM peak hour. All signals along SW 1st Avenue and SW 2nd Avenue are two-phase signals. The signals at the intersection of Jefferson Street at Naito Parkway and Market Street and Naito Parkway are actuated coordinated signals with a 90-second cycle lengths. It was assumed that the cycle lengths and splits would remain unchanged for the traffic operations analysis.

5. OPENING YEAR 2020 TRAFFIC OPERATIONS

Opening year 2020 traffic operations were evaluated for both of the potential sites based on background growth of the existing peak hour volumes. The following section describes the expected traffic operations on the network surrounding the two sites.

2020 Hawthorne Bridgehead Site Operations

Traffic operations near the Hawthorne Bridgehead site are represented by study area intersections one through five between SW 1st and SW 2nd Avenues and SW Madison Street, SW Jefferson Street, and SW Naito Parkway. All five study area intersections around this site are

expected to meet operational standards with an overall intersection LOS of D or better. Operations at the intersections on the corners of the Bridgehead site all operate at a LOS B, with the intersection of SW 2nd Avenue and SW Madison Street operating at LOS C. Although within overall intersection standards, the northbound left from Naito Parkway to Jefferson Street is projected to be overcapacity in the year 2020 PM peak hour. Traffic operations are shown on **Figure 4** and can be found in **Appendix C**.

2020 Block 128 Site Operations

Operations of the Block 128 site are represented by the performance of study area intersections six through 11 between SW 1st and SW 2nd Avenues, SW Naito Parkway, and SW Clay and SW Market Streets. Similar to the Hawthorne Bridgehead site, all of the intersections surrounding the Block 128 site meet operational standards with an overall intersection LOS D or better. Of the intersections directly adjacent to the site, the overall operations for signalized intersections are LOS B or better. The unsignalized intersection of SW 2nd Avenue and SW Clay Street has a STOP controlled through movement on SW 2nd Avenue that experiences LOS D; however, the movement v/c ratio (0.58) indicates that the approach has adequate capacity. Traffic operations are shown on **Figure 4** and can be found in **Appendix C**.

There are no significant concerns or differences with traffic operations at the two proposed sites.

6. PARKING CONSIDERATIONS

The existing courthouse has no parking on-site. The majority of parking for employees and visitors is provided off-site through a variety of public parking lots and garages in the area. Similar to the existing courthouse, the new courthouse will provide no parking. The majority of parking for employees and those using the courthouse will be offsite. Due to the close proximity of both preliminary sites, each site will have access to the same number of parking spots provided by a variety of public parking lots and garages in the area. **Figure 5** below shows the parking availability in the vicinity of both the existing and proposed courthouse sites.

The on-street parking available around each site consists of paid parking for anywhere from 15-minutes to 2-hours. At the Hawthorne Bridgehead site, the only available on-street parking is along SW Jefferson Street. There is space for approximately four to five one-hour parking stalls on the north side of SW Jefferson Street and two 15-minute parking stalls on the south side.

At the Block 128 site, there is parking provided along SW Clay Street, SW 1st Avenue, and SW 2nd Avenue. Along SW Clay Street there is space for four two-hour parking stalls with additional curb space dedicated for motorcycle parking on the north side, and space for five 90-minute stalls and one 15-minute stall on the south side. Parking on SW 1st Avenue is only allowed on the west side where there are five two-hour parking stalls. Parking on SW 2nd Avenue is located on the west side where there are two 15-minute parking stalls. Building on Block 128 will eliminate 150 off-street parking spots

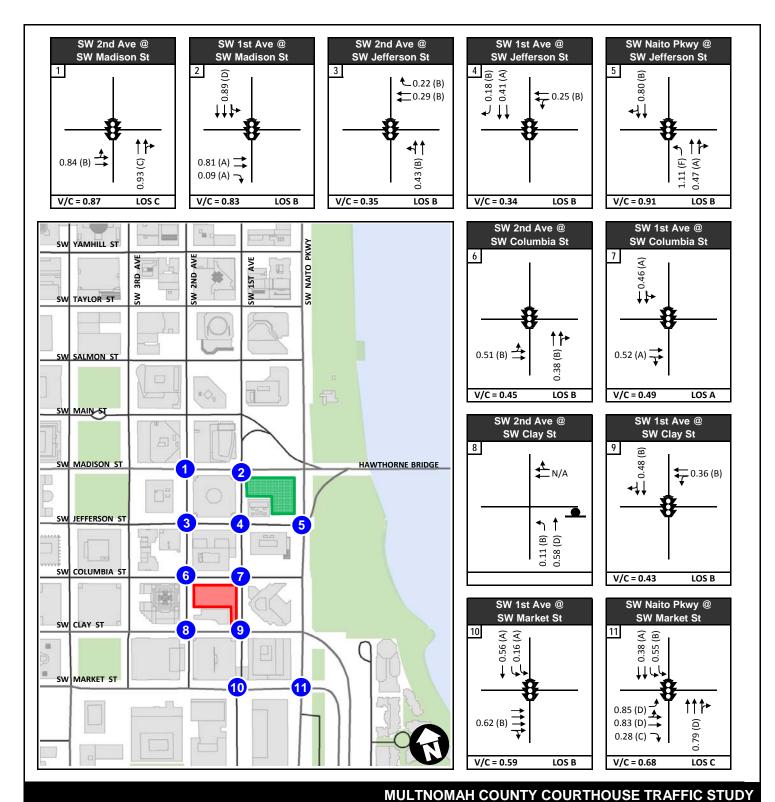
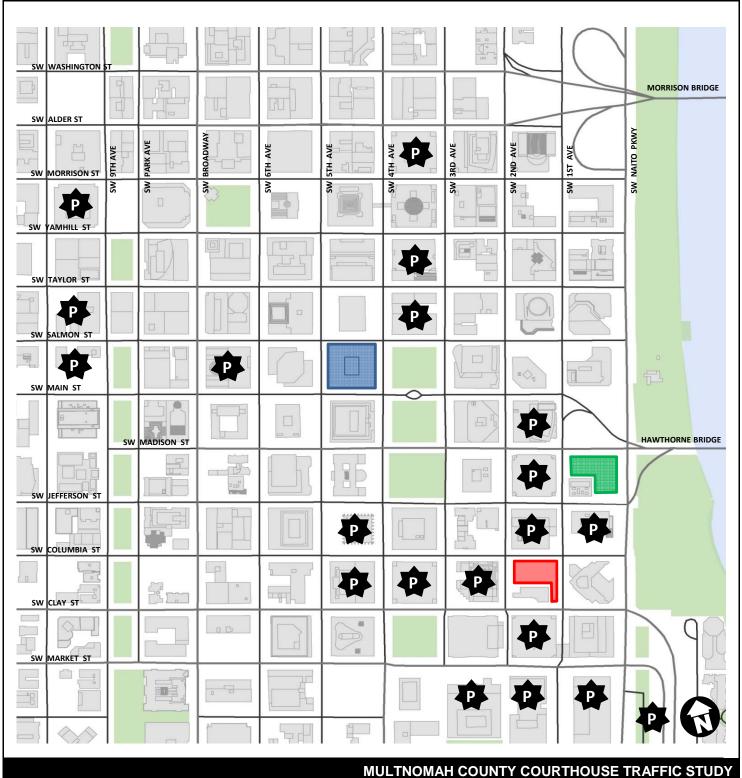


Figure 4 Legend STOP Control Overall LOS and Opening Year (2020) V/C are reported Lane Configurations Signalized Intersection Traffic Operations for signalized intersections. PM Peak Hour Volume-to-capacity Intersection Number Unsignalized intersections only LOS Level of service report V/C and Hawthorne Bridgehead Site LOS for STOP V/C (LOS) #.## (A) controlled Block 128 Site movements. Note: Shape depicts block location only and does not represent the footprint of the proposed courthouse



Legend 1 Intersection Number Available parking Hawthorne Bridgehead Site Block 128 Site Existing Courthouse Note: Shape depicts block location only and does not represent the footprint of the proposed courthouse

While there is more on-street parking available directly adjacent to the Block 128 site, the abundance of off-street parking and nearby on-street parking in close proximity to the two sites indicates there are no significant concerns with parking at the two proposed sites.

7. PEDESTRIAN CONSIDERATIONS

Due to the lack of parking provided on-site, the majority of employees and visitors accessing the site will be pedestrians, traveling to and from available parking resources or transit stops in the vicinity. Pedestrian access to the sites will be from crosswalks at the existing intersections adjacent to the Hawthorne Bridgehead and Block 128 sites. Pedestrian crossings will be unchanged from today. The number of pedestrians using these intersections will increase with addition of the new courthouse. Each site is discussed in more detail below.

Hawthorne Bridgehead

There are currently three intersections that front the Hawthorne Bridgehead site. Of these, the intersections of SW Jefferson Street and SW Madison Street with SW 1st Avenue provide crosswalks on the north, south, east, and west sides of the intersection. The intersection of SW Jefferson Street with SW Naito Parkway has one crosswalk located on the west side of the intersection crossing Jefferson. Because there are no pedestrian crossings of Naito Parkway at Jefferson, pedestrians wishing to access the waterfront would have to walk out of direction to cross SW Naito Parkway at SW Columbia Street, at SW Madison Street via the elevated structure and stairwell, or at the crosswalk at the extension of SW Main Street. Current pedestrian crossings in the area range from 25 to 250 pedestrian crossings per crosswalk in the PM peak hour.

Drivers coming to the Hawthorne Bridgehead site would likely park in a garage to the west or south of the site (see **Figure 5** above). As a result, the two intersections along SW 1st Avenue are likely to see an increase in the number of pedestrians crossing at these signals. This would result in a reduction to vehicular capacity at these intersections and an increase in delay for turning vehicles. Specifically, the dedicated eastbound right turn lane on SW Madison Street approaching the intersection with SW 1st Avenue is likely to experience additional conflicting pedestrian volumes crossing SW 1st Avenue towards the courthouse. Any increases in pedestrian crossings are unlikely to cause significant enough delays to affect the overall performance of the intersections as the right turn is a small fraction of the total intersection volume. Also as a dedicated right-turn lane, queuing in that lane is less likely to impact the adjacent through traffic lanes onto the Hawthorne Bridge.

Block 128

All four corners of Block 128 provide pedestrian crossings. The intersections of SW Columbia Street at SW $1^{\rm st}$ Avenue, SW Columbia Street at SW $2^{\rm nd}$ Avenue, and SW Clay Street at SW $1^{\rm st}$ Avenue have crosswalks on the north, south, east, and west sides of the intersections. The intersection of SW Clay Street at SW $2^{\rm nd}$ Avenue does not provide a striped crosswalk on the

north side of the intersection. There are crosswalks on the south, east, and west side of the intersection.

Drivers coming to the Block 128 site would likely park in a garage to the west, north, or south of the site (see **Figure 5** above). As a result, the two intersections along SW 2st Avenue and the intersection of SW Clay Street at SW 1st Avenue are likely to see an increase in the number of pedestrians crossing at these signals. Current pedestrian crossings are within 50 to 175 pedestrian crossings per crosswalk during the PM peak hour at these intersections. This would result in a reduction to vehicular capacity at these intersections. An increase in conflicting pedestrian movements are not anticipated to increase vehicular delay or reduce capacity to a point where adjacent intersections fail to meet operational standards.

Pedestrian access at the proposed Block 128 site is slightly better than the Hawthorne Bridgehead site due to the limited crossing of Naito Parkway. However, there are no significant concerns with pedestrian access at the two proposed sites.

8. BICYCLE CONSIDERATIONS

Bicycling around the two sites would be unchanged from how cyclists currently use the road. The number of cyclists riding to each site would increase with the new courthouse. Each site will provide bike parking for employees and it is expected to be well utilized. Specifics for each site are discussed below.

Hawthorne Bridgehead

Cyclists in downtown Portland are active users of the travel lane. Cyclists typically do not ride on the sidewalks in downtown. For cyclists coming to the Hawthorne Bridgehead site from the east side of the Willamette River via the Hawthorne Bridge would have to enter the travel lanes from the raised multi-use path and cross two lanes of traffic to make a left on SW 1st Avenue. As alternative to this movement, cyclists could take the designated bicycle and pedestrian exit ramp from the bridge to the at-grade crossing of SW Naito Parkway at the striped crosswalk north of the bridge. Cyclists heading east from the courthouse would be able to access SW Madison Street from SW 1st Avenue and continue across the bike path on the Hawthorne Bridge.

Cyclists on the west side of the Willamette River heading to or from the courthouse will continue to use the downtown grid system. Currently, there is an eastbound right turn lane at the intersection of SW Madison Street and SW 1st Avenue. It is expected that cyclists will use this lane to turn right; however, this is also an active bus stop used by multiple routes. Buses are permitted to go straight from the right turn lane through the intersection towards the Hawthorne Bridge. The striped bike lane for this block is between the through lane and the right turn lane. With the additional cyclists trying to reach the courthouse, this could increase the potential for conflicts between cyclists trying to turn right in front of buses accessing the Hawthorne Bridge from the curb-tight bus stop. When the Tilikum Crossing and new Sellwood Bridge open, lines 31, 32, 33 and 99 will no longer stop at this bus stop.

There is also a right turn lane along SW 1st Avenue at the intersection with SW Jefferson Street. The bike lane is striped between the through and the right turn lane. Again, the increase in the number of cyclists in this area may increase the potential for conflict between vehicles crossing over the bike lane.

Block 128

Block 128 is surrounded by four one-way streets. Bicyclists heading to or from the courthouse will continue to use the downtown grid system. There are no right turn lanes on the adjacent roadways. Bicyclists are expected to be traveling in the vehicular lane or on the outside of vehicular traffic. The building fronts along SW 1st Avenue and SW Clay Street currently have on street parking. The increased number of cyclists will increase the number of parking/bicycle conflicts surrounding the block.

Bicycle operations at the proposed Block 128 site is slightly better than the Hawthorne Bridgehead site due more standard roadway grid and reduced bus conflict points. However, there are no significant concerns with bicycle operations at the two proposed sites.

9. TRANSIT CONSIDERATIONS

Hawthorne Bridgehead

The Hawthorne Bridgehead site is currently serviced by 13 bus lines and is within five blocks of the blue, red, green, and yellow MAX lines. Bus lines 4, 6, 10, 14, 31, 32, 33, and 99 all utilize the Hawthorne Bridge and have stops along SW Madison and SW Main Streets. Lines 38, 45, 55, 92, and 96 run along SW Naito Parkway/SW Jefferson Street and SW Columbia Street/SW 1st Avenue. When the Tilikum Crossing opens, lines 31, 32, and 33 will no longer service downtown Portland. Current users would be expected to transfer to the MAX orange line. In addition, line 99 would be rerouted from the Hawthorne Bridge and moved to the Sellwood Bridge via Macadam Avenue once the Sellwood Bridge opens to bus traffic. The rerouting of these four bus lines will reduce bus frequency at the stop on Madison Street adjacent to the site.

Block 128

The Block 128 site is currently serviced by 13 bus lines within three blocks and is within six blocks of the blue, red, green and yellow MAX lines. Bus lines 4, 6, 10, 14, 31, 32, 33, and 99 all utilize the Hawthorne Bridge and have stops along SW Madison and SW Main Streets. Lines 38, 45, 55, 92, and 96 run along SW Naito Parkway/SW Jefferson Street and SW Columbia Street/SW 1st Avenue.

Transit access at the proposed sites are similar. There are no significant concerns with transit access at the two proposed sites.

10. SITE ACCESS CONSIDERATIONS

The only vehicle access provided to the new courthouse at either the Hawthorne Bridgehead or the Block 128 sites will be via a sally port. For the Hawthorne Bridgehead site, vehicles will enter from southbound SW Naito Parkway and exit onto SW Jefferson Street. At Block 128, vehicles will enter from SW 2nd Avenue and exit onto SW Columbia Street. The sally port is expected to have four trips per day for secure prisoner transfers. One trip will occur during the AM peak, two will occur mid-day, and the last trip will be during the PM peak hour. Given the very low volume, vehicle access at either proposed site is not a concern. Compared to the existing courthouse where SW 5th Avenue is be closed during prisoner transfers, the sally port will significantly improve vehicle access by having a secure location off-street to transfer prisoners which will not require street closures.

11. FREIGHT LOADING CONSIDERATIONS

The sally port access has been provided for secure prisoner transfers at the new courthouse. It is possible the County could use the sally port for freight delivery. This option would be further explored during the design of the site. If the sally port can't be used for freight, deliveries are expected to be similar to the existing courthouse. The existing Multnomah County Courthouse has dedicated a portion of the on-street parking to be for freight delivery between 7 AM and 7 PM. For the Hawthorne Bridgehead site, there is existing freight delivery located along SW Jefferson Street between 7 AM and 7 PM. For Block 128 there is not existing freight delivery signed adjacent to the block. There is a freight delivery zone across the street on the west side of SW 2nd Avenue.

If the sally ports cannot be used for freight loading, the existing loading zone on SW Jefferson Street at the Hawthorne Bridgehead site could potentially be used, or reconfigured, to accommodate truck deliveries to the new courthouse. Since the existing loading zone at the Block 128 site is across the street, it is likely that a new loading zone would have to be identified for Block 128. In any case, the loading zone will have to be located in a place onstreet that is conducive to the new courthouse building design, which may require new loading zone locations.

12. TEMPORARY CONSTRUCTION IMPACTS

For the purposes of this Transportation Alternatives Analysis, it is assumed that the contractor will need to close one lane on multiple block faces adjacent to the proposed sites. The temporary lane closures present specific issues at each location.

Hawthorne Bridgehead

The Hawthorne Bridgehead is enclosed by SW Madison Street on the north, SW Jefferson Street on the south, SW 1^{st} Avenue on the west, and SW Naito Parkway on the east. The contractor would likely close lanes on SW 1^{st} Avenue and SW Jefferson Street. It is unlikely the City of

Portland would permit the contractor to close lanes along SW Madison Street and SW Naito Parkway during the peak hours, restricting lane closures to the nighttime and midday periods. Exact hours of closures will need to be coordinated with the City of Portland Bureau of Transportation and the County will require the Contractor to work with the adjacent building owner's to minimize impacts to their on-going operations.

Closing one lane adjacent to the site will interfere with the four one-hour on-street parking stalls, truck loading zone and bus stop on SW Jefferson Street, but would not result in a loss of travel lane. Blocking the bus stop and truck loading zones may require trucks and buses to reroute to temporary transit stops and loading zones for the duration of construction. Lane closures on SW 1st Avenue would result in the loss of a travel lane during construction.

Construction staging will occur at the North Triangle for lay down/stating areas. It is also possible the contractor may use the top of the City Garage for lighter materials.

Block 128

The Block 128 site is enclosed by SW Columbia Street on the north, SW Clay Street on the south, SW 2nd Avenue on the west, and SW 1st Avenue on the east. It is unlikely the City of Portland would permit the contractor to take lanes along SW Clay Street during the peak hours, restricting lane closures to the nighttime and midday periods. Exact hours of closures will need to be coordinated with the City of Portland Bureau of Transportation.

Closing the lanes adjacent to the Block 128 site will interfere with a bus stop on SW Columbia Street which will require the bus stop to be relocated to a nearby location. Additionally, six two-hour on-street parking stalls on SW 1st Avenue, and four two-hour on-street parking stalls and on-street motorcycle parking on SW Clay Street will be affected by temporary lane closures. The driveway to the existing underground parking and freight loading area located on-site is also accessed from SW Clay Street and would likely have to be maintained for operations during construction. Lane closures would result in the loss of a travel lane on SW 2nd Avenue.

Construction staging for this site is to be determined.

There are no significant concerns or differences with construction impacts to traffic at the two proposed sites.

13. CONCLUSIONS

The relocated courthouse is not expected to alter downtown traffic patterns or operations significantly. It is assumed that the trips generated for the new courthouse will be comparable to the trips generated by the existing courthouse; therefore no net new trips are expected to be added to the downtown network. Traffic operations for the 2020 opening year volume forecasts, based on background growth rates, indicate that all study area intersections are expected to operate within the overall intersection LOS D standard for signalized intersections and LOS E standard for unsignalized intersections.

Due to the close proximity of the two proposed sites and the availability of off-site parking around both, travel patterns for commuters and visitors are expected to be similar for both sites. Adjacent intersections at either location should expect increases in pedestrian and bicycle crossings which may reduce the vehicular capacity of conflicting turning movements and increases in delay. The effects of this increased pedestrian and bicycle activity pose unique challenges for each location, but are not expected to affect the overall traffic operations for any study area intersections significantly.

Temporary traffic impacts due to construction will require the contractor to block travel lanes or on-street parking lanes for both locations. The specific impacts are unique to each site, but may both result in loss of on-street parking, through lane capacity, relocated bus stops, and time-of-day restrictions for travel lane closures on major roadways.

In summary, the transportation analysis for the two proposed sites does not preclude either site from consideration as there are no fatal flaws with respect to transportation for either site.

APPENDIX A – Traffic Counts

Project: Job #: Hawthorne Bridge Mult00000-049

Subject: PM Turning Movement Volumes
Created: 3/2/2015
Rev. Date: 3/6/2015

| E-W ID | Synchro ID | Intersection | Direction | Movement | Int ID | 4:00 PM | 4:15 PM | 4:30 PM | 4:45 PM | 5:00 PM | 5:15 PM | 5:30 PM | 5:45 PM | Max | Hour | Delta | USE |] [| Bikes | Pe | ds |
|--------|----------------------|--|-----------|--------------------------|----------------------|------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------|---------|-------|--------------------------|-----|--------------------|-------|-------------------|
| 1 | 10 10 10 | SW 2nd Ave @SW Madison St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 10 10 10 | 24 233 0 | 19 270 0 | 20 285 0 | 22 279 0 | 17 317 0 | 11 330 0 | 10 337 0 | 15 297 0 | | | | 60 1263 0 | | 0 214 0 | North | 130 |
| | 10 10 | 2015 | WB | WBL WBT WBR | 10 10 10 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | | | | 0 0 | • | 0 0 1 | South | 246 |
| | 10 10 10 10 | PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 0 | NB | NBL NBT NBR | 10 10 10 | 0 87 62 | 0 76 56 | 0 102 51 | 0 106 58 | 0 98 49 | 0 103 63 | 0 105 64 | 0 73 60 | | | | 0 412 234 | • | 0 13 16 | East | 247 |
| | 10 10 | PHF: 0.95 | SB | SBL SBT SBR | 10 10 10 10 | 0 0 0 | 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 | | | | 0 0 0 | • | 15 0 0 | West | 157 |
| | 10 | 0.95 | TEV | SBR | 10 | 406 | 827 | 1285 | 1750 | 1825 | 1911 | 1969 | 1949 | 1969 | 5:30 PM | 0 | 1969 | | 259 | | 780 |
| 2 | 20 20 20 | SW 1st Ave @SW Madison St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 20 20 20 | 0 263 22 | 0 303 22 | 0 314 21 | 0 320 22 | 0 340 17 | 0 378 16 | 0 380 19 | 0 344 15 | | | | 0 1418 74 | • | 0 252 3 | North | 23 |
| | 20 20 20 | 2015 | WB | WBL WBT WBR | 20 20 20 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | | | | 0 0 0 | | 0 0 0 | South | 103 |
| | 20 20 20 20 | PM Peak Hour: 5:00 PM-6:00 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 23 | NB | NBL NBT NBR SBL | 20 20 20 20 | 0 0 0 26 | 0 0 0 27 | 0 0 0 33 | 0 0 0 30 | 0 0 0 25 | 0 0 0 42 | 0 0 0 40 | 0 0 0 43 | | | | 0 0 0 | | 0 0 5 | East | 91 |
| | 20 20 20 | PHF: 0.95 | SB | SBT SBR | 20 20 20 | 136 0 447 | 130 0 929 | 155 0 1452 | 149 0 1973 | 166 0 2074 | 151 0 2179 | 140 0 2235 | 142 0 2258 | 2258 | 5:45 PM | 23 | 606 0 2235 | | 13 1 290 | West | 235 452 |
| 3 | 30 | SW 2nd Ave @SW Jefferson St | | EBL | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2200 | 0.401 m | | 0 | | 0 | | 702 |
| | 30 30 30 | 2 hr PM Turning Movement Count Count Date: 2/26/2015 2015 | EB | EBT EBR WBL | 30 30 30 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 | 0 0 0 | | | | 0 0 0 | | 0 0 0 | North | 39 |
| | 30 30 30 30 | PM Peak Hour: 4:30 PM-5:30 PM | WB NB | WBT WBR NBL NBT | 30 30 30 | 97 66 19 87 | 97 47 24 91 | 102 75 33 83 | 98 67 35 92 | 117 63 27 | 80 79 28 | 77 49 23 | 83 33 18 | | | | 372 258 113 376 | | 12 5 3 | South | 79 |
| | 30 30 30 30 | PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 29 PHF: | SB | NBT NBR SBL SBT | 30 30 30 30 | 0 0 0 | 91 0 0 | 0 0 0 | 92 0 0 0 | 88 0 0 | 81 0 0 | 115 0 0 | 100 0 0 | | | | 0 0 0 | • | 26 0 0 | West | 164 |
| | 30 | 0.95 | TEV | SBR | 30 | 0 269 | 0 528 | 0 821 | 0 1113 | 0 1139 | 0 1148 | 0 1119 | 0 | 1148 | 5:15 PM | 29 | 0 1119 | | 0 | West | 77 359 |
| 4 | 40 40 | SW 1st Ave @SW Jefferson St 2 hr PM Turning Movement Count | EB | EBL EBT | 40 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | | 0 | North | |
| | 40 40 40 | Count Date: 2/26/2015 2015 | WB | EBR WBL WBT | 40 40 40 | 0 11 48 | 0 11 49 | 0 13 67 | 0 12 44 | 0 21 66 | 0 17 59 | 0 12 40 | 0 12 40 | | | | 0 62 209 | | 6 6 | South | 75 |
| | 40 40 40 | PM Peak Hour: 4:30 PM-5:30 PM PM Peak Hour Used: 4:45 PM-5:45 PM | NB | WBR NBL NBT | 40 40 40 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | | | | 0 0 | | 0 | East | 76 |
| | 40 40 40 40 | Volume Difference: 52 PHF: 0.86 | SB | NBR SBL SBT SBR | 40 40 40 40 | 0 0 106 59 | 0 0 113 42 | 0 0 119 57 | 0 0 109 58 | 0 0 133 54 | 0 0 130 38 | 0 0 124 28 | 0 0 107 46 | | | | 0 0 496 178 | • | 0 0 11 5 | West | 168 |
| | 40 | 0.00 | TEV | SDIV | 40 | 224 | 439 | 695 | 918 | 968 | 997 | 945 | 927 | 997 | 5:15 PM | 52 | 945 | | 32 | | 504 |
| 5 | 50 50 50 | SW Naito Pkwy @SW Jefferson St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 50 50 50 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | | | | 0 0 0 | | 0 0 0 | North | 1 |
| | 50 50 50 | 2015 | WB | WBL WBT WBR | 50 50 50 | 0 | 0 0 | 0 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | | | | 0 0 | | 0 | South | 0 |
| | 50 50 50 | PM Peak Hour: 4:00 PM-5:00 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 98 | NB | NBL NBT NBR | 50 50 50 | 20 242 119 | 33 256 104 | 27 267 104 | 27 253 94 | 31 261 99 | 21 266 95 | 14 245 71 | 16 206 76 | | | | 93 1025 359 0 | | 2 6 5 | East | 0 |
| | 50 50 50 | PHF: 0.96 | SB | SBL SBT SBR | 50 50 50 | 0 339 34 754 | 0 315 21 1483 | 0 320 43 2244 | 0 318 26 2962 | 0 319 36 2954 | 0 313 36 2956 | 0 309 30 2864 | 0 280 28 2752 | 2962 | 4:45 PM | 98 | 1259 128 2864 | | 0 3 12 28 | West | 16 17 |
| | | | I IEV | · · | | 134 | 1403 | 2244 | 2902 | 2934 | 2930 | 2004 | 2132 | 2902 | 4:45 PM | 90 | 2004 | | 20 | | - 17 |

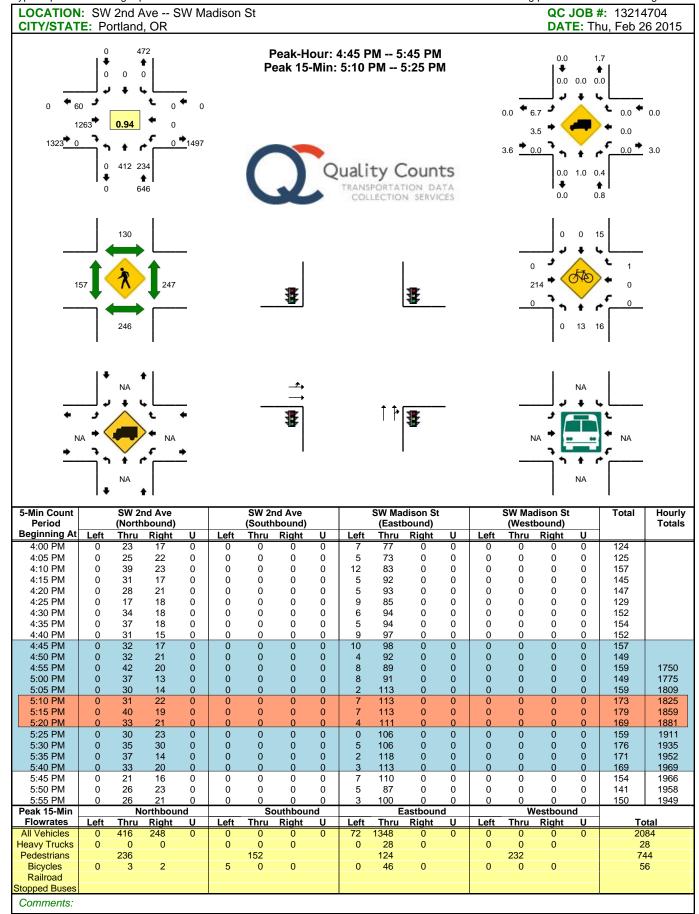
PM_MC_Courthouse_Vol_Dev_03-02-15.xlsm:PM Count Data Page 1 of 2 Project: Job #: Hawthorne Bridge Mult00000-049

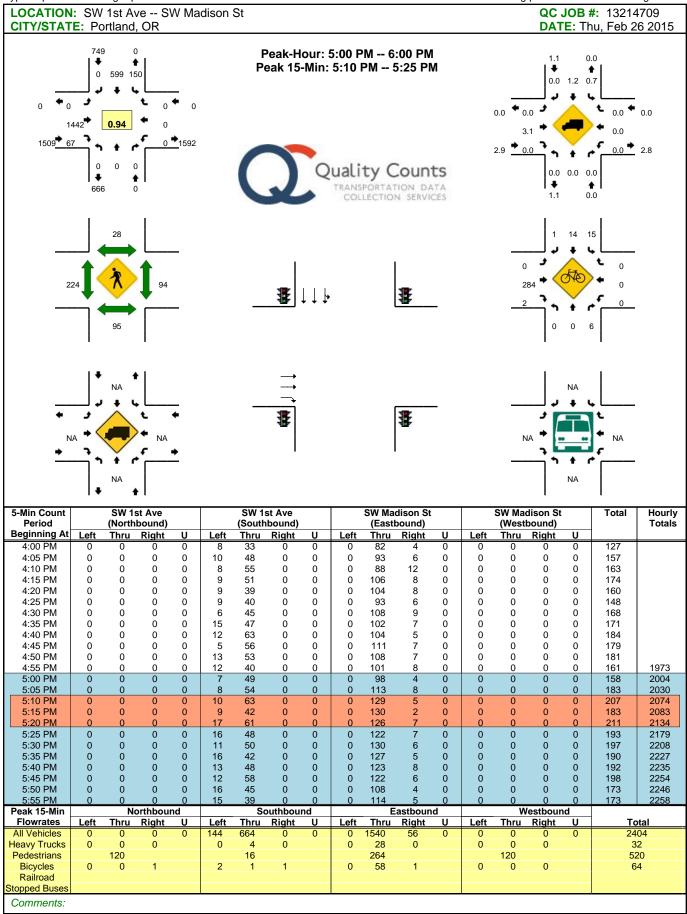
Subject: PM Turning Movement Volumes
Created: 3/2/2015
Rev. Date: 3/6/2015

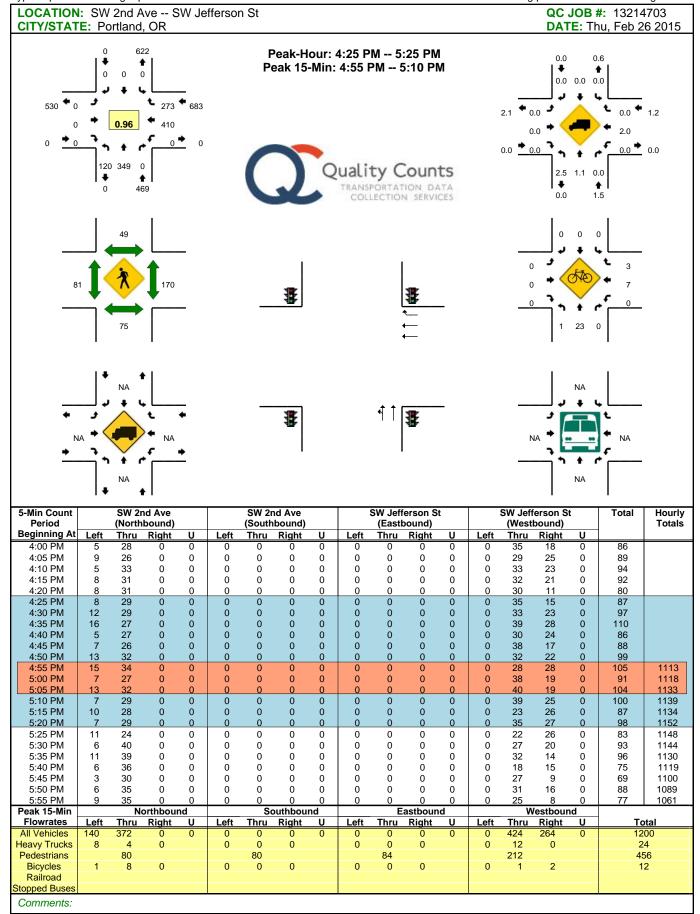
PM_MC_Courthouse_Vol_Dev_03-02-15.xlsm:PM Count Data

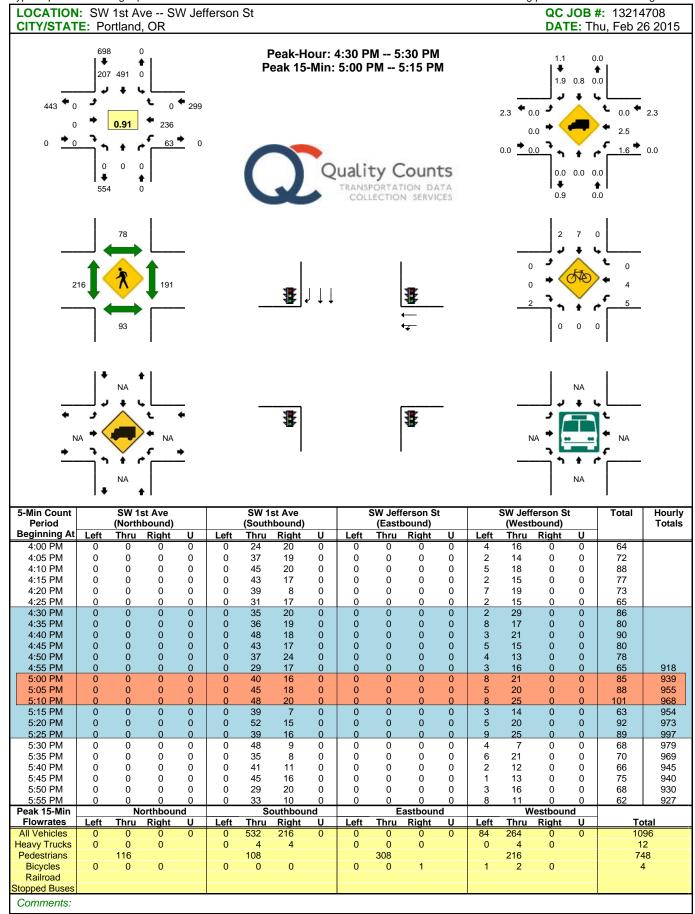
| E-W ID | Synchro ID | Intersection | Direction | Movement | Int ID | 4:00 PM | 4:15 PM | 4:30 PM | 4:45 PM | 5:00 PM | 5:15 PM | 5:30 PM | 5:45 PM | Max | Hour | Delta | USE | Bikes | Pe | ds |
|--------|----------------------|---|----------------|----------------------------------|-------------------|--------------------|--------------------|---------------------|---------------------|--------------------|--------------------|---------------------|---------------------|-------|---------|-------|-------------------|-----------------|-------|------------------|
| 6 | 60 60 60 | SW 2nd Ave @SW Columbia St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 60 60 | 23 110 0 | 32 113 0 | 23 112 0 | 36 134 0 | 29 130 0 | 37 134 0 | 30 137 0 | 37 102 0 | | | | 132 535 0 | 4 31 0 | North | 117 |
| | 60 60 | 2015 | WB | WBL WBT | 60 60 60 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | South | |
| | 60 60 60 | PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM | NB | WBR NBL NBT | 60 60 | 0 0 86 | 0 85 | 0 95 | 0 0 84 | 0 0 91 | 0 0 80 | 0 91 | 0 | | | | 0 0 346 | 0 23 | East | 114 |
| | 60 60 60 | Volume Difference: 0 PHF: | SB | NBR SBL SBT | 60 60 60 | 0 0 | 0 0 | 15 0 0 | 0 0 | 17 0 0 | 17 0 0 | 16 0 0 | 0 0 | | | | 72 0 0 | 0 0 | West | 116 |
| | 60 | 0.98 | TEV | SBR | 60 | 0 240 | 0 484 | 729 | 0 1005 | 0 1032 | 0 1056 | 0 1085 | 0 1041 | 1085 | 5:30 PM | 0 | 0 1085 | 0 69 | | 97 444 |
| 7 | 70 70 70 | SW 1st Ave @SW Columbia St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 70 70 70 | 0 106 25 | 0 97 28 | 0 97 33 | 0 113 43 | 0 101 49 | 0 117 35 | 0 115 38 | 0 80 30 | | | | 0 446 165 | 0 39 0 | North | 119 |
| | 70 70 70 | 2015 | WB | WBL WBT WBR | 70 70 70 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | | | | 0 0 | 0 2 0 | South | 116 |
| | 70 70 70 | PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 0 | NB | NBL NBT NBR | 70 70 70 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | | | | 0 | 0 0 | East | 143 |
| | 70 70 70 70 | PHF: 0.95 | SB | SBL SBT SBR | 70 70 70 | 26 92 0 | 33 91 0 | 36 93 0 | 28 106 0 | 38 119 0 | 34 112 0 | 23 101 0 | 24 94 0 | | | | 123 438 0 | 5 13 0 | West | 168 |
| | | | TEV | | | 249 | 498 | 757 | 1047 | 1105 | 1154 | 1172 | 1110 | 1172 | 5:30 PM | 0 | 1172 | 59 | | 546 |
| 8 | 80 80 80 | SW 2nd Ave @SW Clay St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 80 80 80 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 | | | | 0 0 0 | 1 0 0 | North | 57 |
| | 80 80 80 | 2015 | WB | WBL WBT WBR | 80 80 80 | 0 96 64 | 0 110 60 | 0 101 72 | 0 89 63 | 0 89 63 | 0 78 55 | 0 91 49 | 0 85 60 | | | | 0 347 230 | 0 4 4 | South | 70 |
| | 80 80 80 | PM Peak Hour: 4:15 PM-5:15 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 39 | NB | NBL NBT NBR | 80 80 80 | 17 37 0 | 16 32 0 | 14 35 0 | 10 40 0 | 26 43 0 | 12 52 0 | 16 48 0 | 6 38 0 | | | | 64 183 0 | 1 29 0 | East | 93 |
| | 80 80 80 | PHF: 0.93 | SB | SBL SBT SBR | 80 80 80 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 | 0 0 | | | | 0 | 0 0 | West | 98 |
| | | | TEV | | | 214 | 432 | 654 | 856 | 863 | 842 | 824 | 811 | 863 | 5:00 PM | 39 | 824 | 39 | | 318 |
| 9 | 90 90 90 | SW 1st Ave @SW Clay St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 90 90 90 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | | | | 0 0 0 | 0 0 0 | North | 69 |
| | 90 90 90 | 2015 | WB | WBL WBT WBR | 90 90 90 | 9 110 0 | 14 113 0 | 17 94 0 | 11 98 0 | 16 83 0 | 9 85 0 | 8 96 0 | 7 105 0 | | | | 44 362 0 | 2 1 0 | South | 105 |
| | 90 90 90 | PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 0 | NB | NBL NBT NBR | 90 90 90 | 0 0 | 0 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 000 | 0 0 0 | | | | 0 0 0 | 2 0 0 | East | 132 |
| | 90 90 90 | PHF: 0.96 | SB | SBL SBT SBR | 90 90 90 | 0 89 26 | 0 95 26 | 0 98 35 | 0 117 21 | 0 133 30 | 0 133 16 | 0 142 19 | 0 106 20 | | | | 0 525 86 | 0 13 3 | West | 143 |
| | | | TEV | | | 234 | 482 | 726 | 973 | 1001 | 996 | 1017 | 1008 | 1017 | 5:30 PM | 0 | 1017 | 21 | | 449 |
| 10 | 100 100 100 | SW 1st Ave @SW Market St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 100 100 100 | 0 232 98 | 0 204 86 | 0 196 80 | 0 193 89 | 0 221 100 | 0 225 94 | 0 191 94 | 0 156 69 | | | | 0 830 377 | 0 25 1 | North | 35 |
| | 100 100 100 | 2015 | WB | WBL WBT WBR | 100 100 100 | 0 | 0 0 0 | 0 | 0 0 | 0 | 0 | 000 | 0 0 0 | | | | 0 0 0 | 0 0 | South | 34 |
| | 100 100 100 | PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 0 | NB | NBL NBT NBR | 100 100 100 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | | | | 0 0 | 0 1 9 | East | 90 |
| | 100 100 100 | PHF: 0.94 | SB | SBL SBT SBR | 100 100 100 | 47 44 0 | 50 62 0 | 43 67 0 | 41 91 0 | 61 90 0 | 50 92 0 | 52 99 0 | 47 65 0 | | | | 204 372 0 | 1 14 0 | West | 81 |
| | | | TEV | | | 421 | 823 | 1209 | 1623 | 1674 | 1733 | 1783 | 1706 | 1783 | 5:30 PM | 0 | 1783 | 51 | | 240 |
| 11 | 110 110 110 | SW Naito Pkwy @SW Market St 2 hr PM Turning Movement Count Count Date: 2/26/2015 | EB | EBL EBT EBR | 110 110 110 | 69 131 75 | 65 114 84 | 67 117 56 | 80 101 62 | 87 133 65 | 94 120 55 | 80 119 43 | 51 102 52 | | | | 341 473 225 | 30 0 0 | North | 20 |
| | 110 110 110 | 2015 | WB | WBL WBT WBR | 110 110 110 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 | 0 0 0 | 0 0 0 | 0 0 | 0 0 0 | | | | 0 0 0 | 0 0 | South | 21 |
| | 110 110 110 | PM Peak Hour: 4:00 PM-5:00 PM PM Peak Hour Used: 4:45 PM-5:45 PM Volume Difference: 145 | NB | NBL NBT NBR | 110 110 110 | 0 161 6 | 0 167 3 | 0 185 3 | 0 143 4 | 0 129 6 | 0 134 1 | 0 115 1 | 0 134 4 | | | | 0 521 12 | 0 18 0 | East | 35 |
| | 110 110 110 | PHF: 0.96 | SB | SBL SBT SBR | 110 110 110 | 210 187 0 | 176 213 0 | 178 226 0 | 196 192 0 | 202 192 0 | 183 216 0 | 188 185 0 | 171 171 0 | | | | 769 785 0 | 0 0 | West | 7 |
| | | | TEV | | | 839 | 1661 | 2493 | 3271 | 3246 | 3227 | 3126 | 3033 | 3271 | 4:45 PM | 145 | 3126 | 48 | | 83 |
| | | Intersection Totals | EB WB NB | Approach Approach Approach | | 1411 501 964 | 1437 501 787 | 1421 541 826 | 1494 482 821 | 1606 518 830 | 1646 462 818 | 1593 422 808 | 1350 425 686 | | | | | | | |
| | | | SB TEV | Approach I hr | L | 1421 4297 | 893 7915 | 989 11692 | 962 15451 | 1053 15161 | 1005 15474 | 956 15476 | 890 15068 | 15476 | 5:30 PM | 0 | 12:00 AM | | | |
| | | | | | | | | | | | | Peak Hour | | | | | | | | |

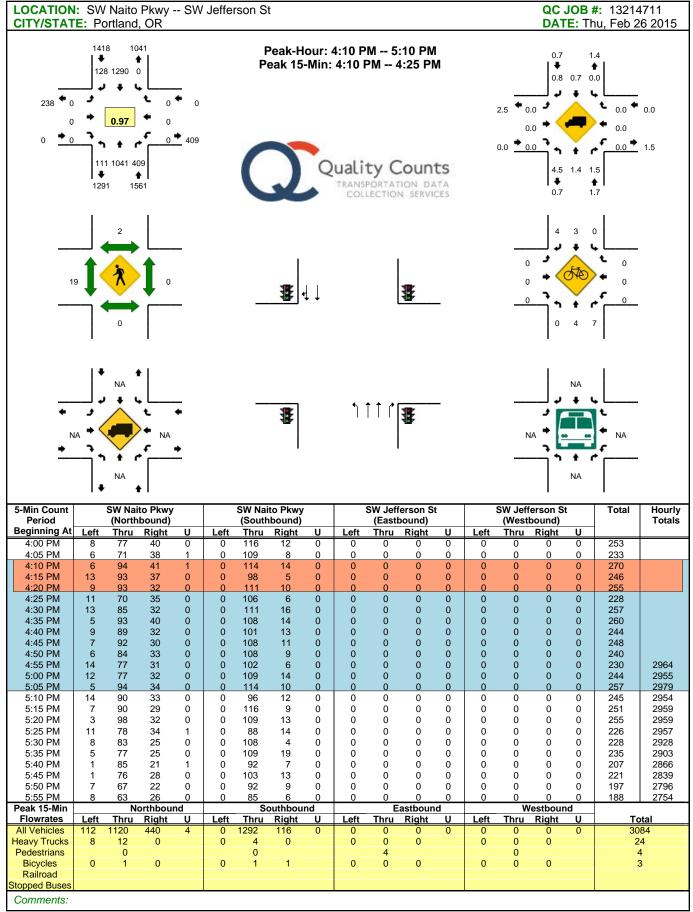
Page 2 of 2

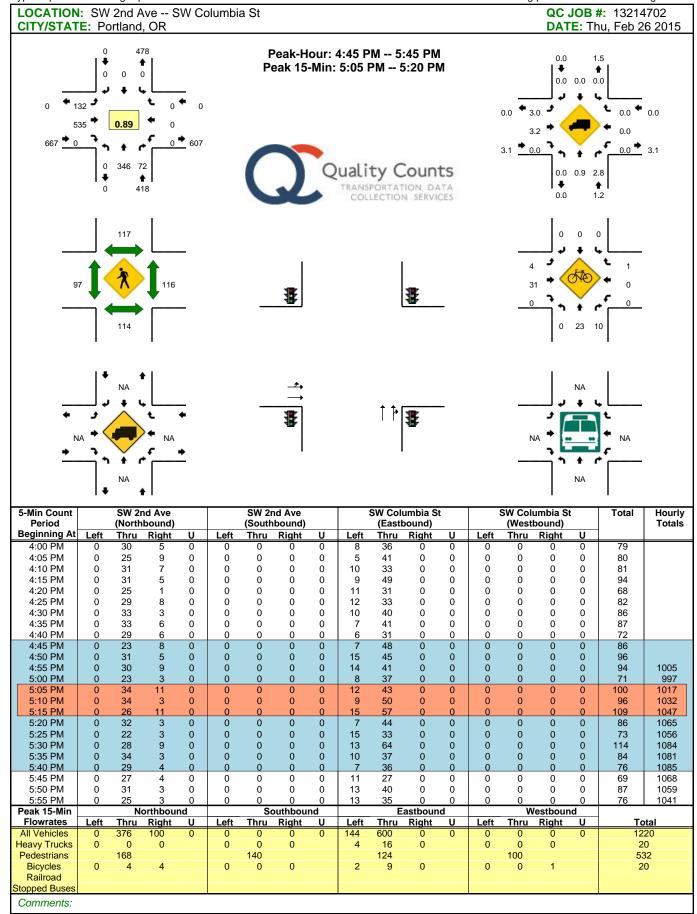


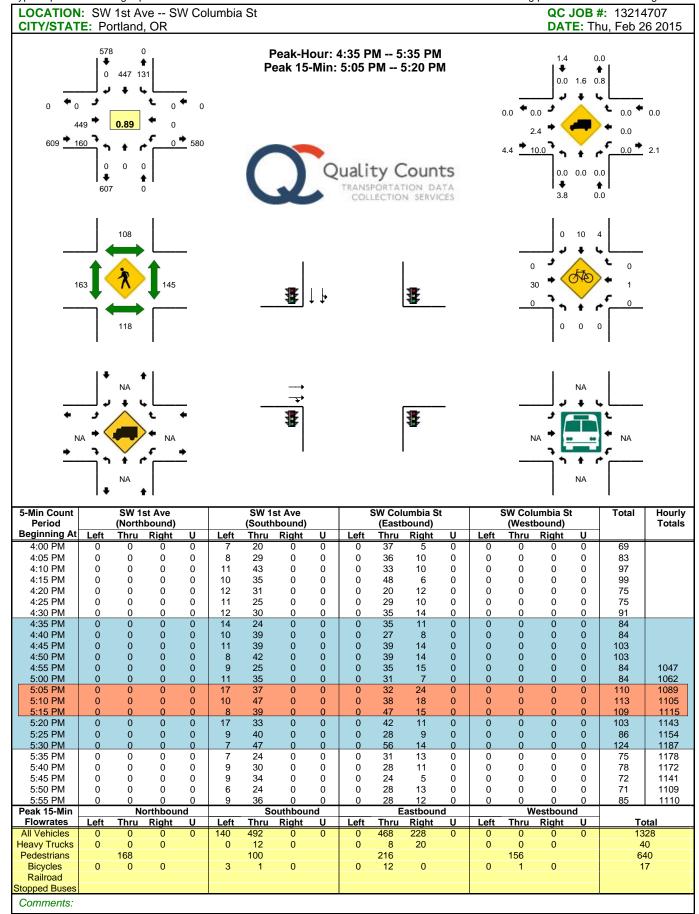


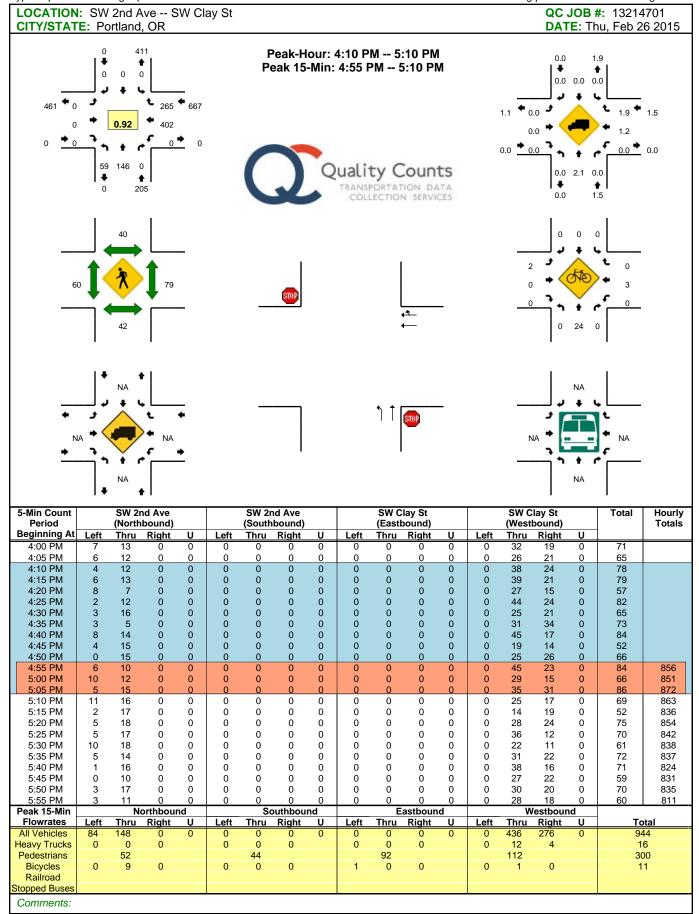


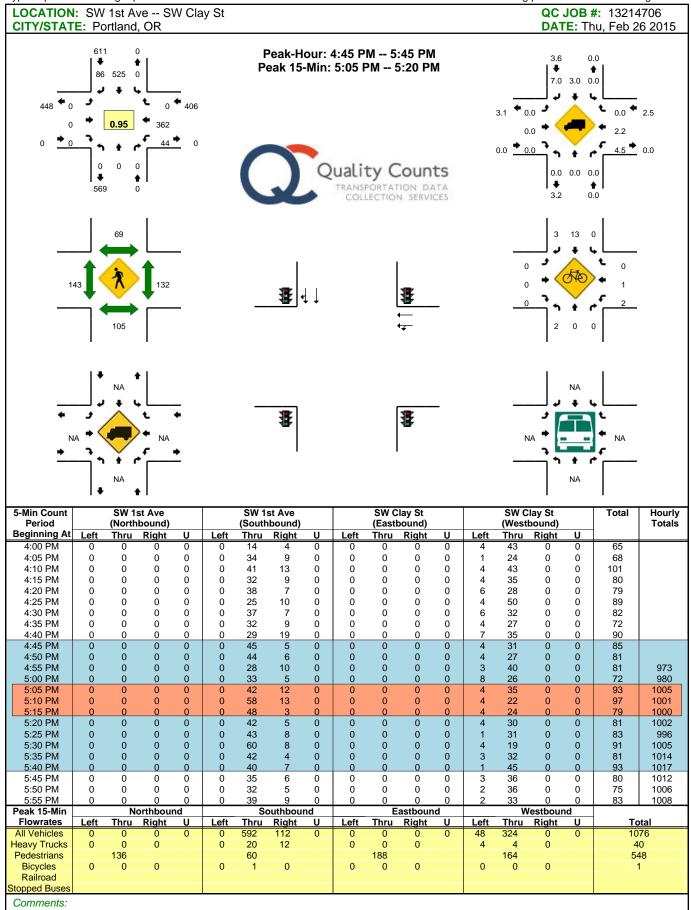


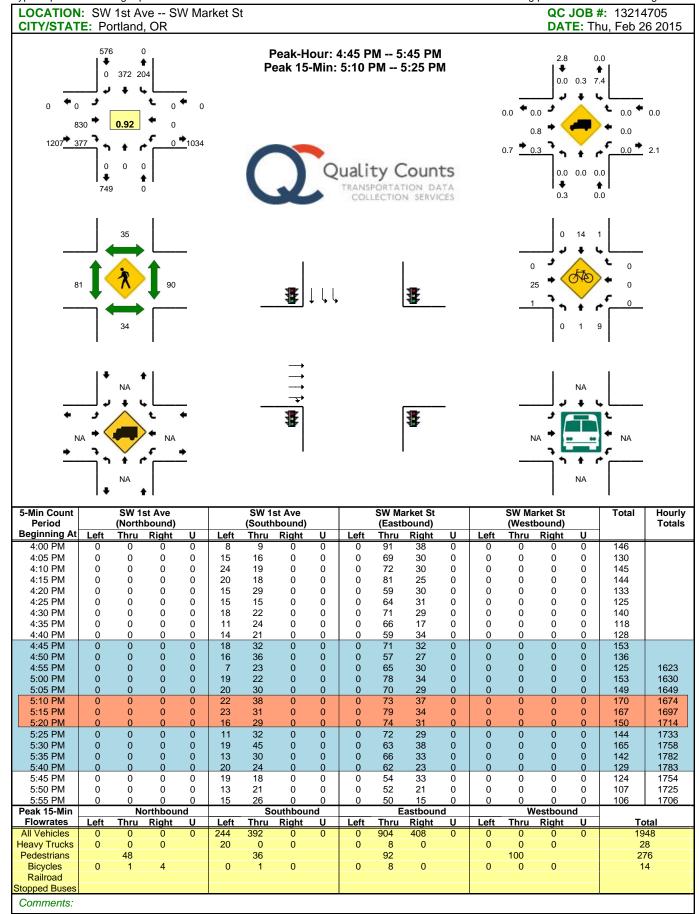


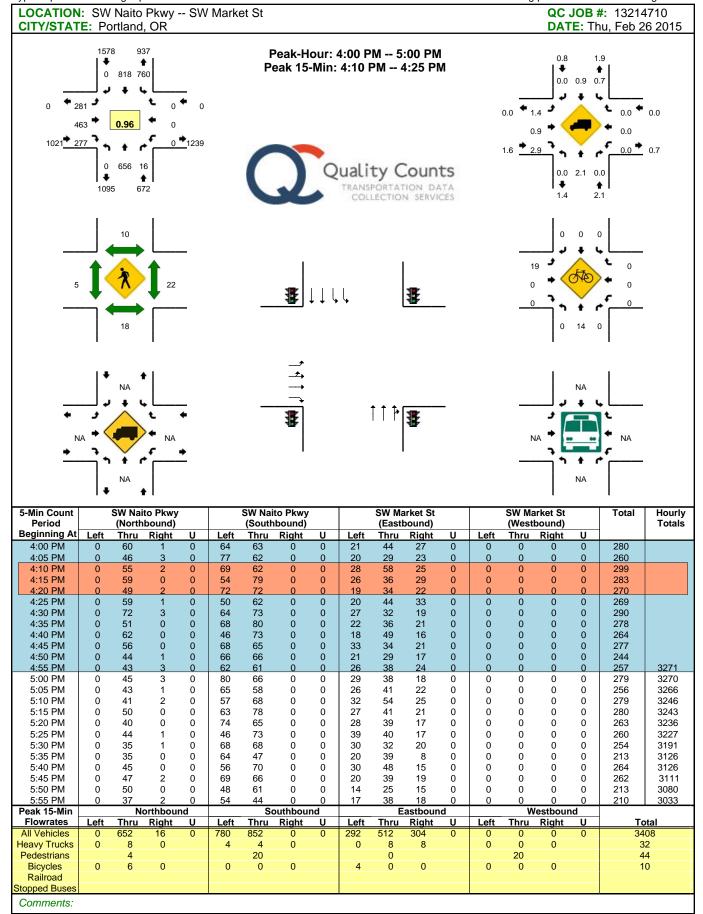












APPENDIX B – Volume Development

Project: Job #: Subject: Multnomah County Courthouse MULT0000-0072 PM Turning Movement Volumes Growth Rate = Updated - 3/3/2015

| Created: | 3/2/2015 | , | | | | | | | 1% | | |
|------------|------------------------|---|-----------|------------|-----------------|---|--|---|---------------------------------------|---------------------------------|-------------------------------------|
| Rev. Date: | 3/6/2015 Synchro ID | Intersection | Direction | Movement | Int ID | Existing Counts 2015 1-Hr Volume PM Peak | Existing 2015 Heavy Vehicle Count | Existing 2015 Heavy Vehicle Percentage | 2020 Unbalanced Volumes PM Peak | Volume Balancing Adjustments | 2020 Balanced Volumes PM Peak |
| | | | | | | | | | | | |
| 1 | 10 | SW 2nd Ave @SW Madison St | 1 | EBL | 10 | 60 | 4 | 7% | 65 | 0 | 65 |
| | 10 | 2 hr PM Turning Movement Count | EB | EBT | 10 | 1263 | 44 | 3% | 1325 | 0 | 1325 |
| | 10 | Count Date: 2/26/2015 | <u> </u> | EBR | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 10 10 | 2015 Signalized | WB | WBL WBT | 10 10 | 0 | 0 | 0% 0% | 0 | 0 | 0 |
| | 10 | Signalized | WD | WBR | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 10 | PM Peak Hour: 4:45 PM-5:45 PM | | NBL | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 10 | PM Peak Hour Used: 4:45 PM-5:45 PM | NB | NBT | 10 | 412 | 4 | 1% | 435 | 0 | 435 |
| | 10 | T WT CURTION COCK. 4.40 T W C.40 T W | 110 | NBR | 10 | 234 | i | 0% | 245 | ő | 245 |
| | 10 | | | SBL | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 10 | PHF: | SB | SBT | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 10 | 0.95 | | SBR | 10 | 0 | 0 | 0% | 0 | 0 | 0 |
| | | | TEV | TEV | 10 | 1969 | 53 | | 2070 | 0 | 2070 |
| 0 | - 00 | SW 1st Ave @SW Madison St | | - FDI | 00 | 0 | | 0% | | | 0 |
| 2 | 20 20 | 2 hr PM Turning Movement Count | EB | EBL EBT | 20 20 | 0 1418 | 0 44 | 0% 3% | 0 1490 | 0 0 | 0 1490 |
| | 20 | Count Date: 2/26/2015 | ED | EBR | 20 | 74 | 0 | 0% | 80 | 0 | 80 |
| | 20 | 2015 | | WBL | 20 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 20 | Signalized | WB | WBT | 20 | 0 | 0 | 0% | 0 | Ō | 0 |
| | 20 | _ | | WBR | 20 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 20 | PM Peak Hour: 5:00 PM-6:00 PM | | NBL | 20 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 20 | PM Peak Hour Used: 4:45 PM-5:45 PM | NB | NBT | 20 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 20 | | | NBR | 20 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 20 | | | SBL | 20 | 137 | 2 | 1% | 145 | 0 | 145 |
| | 20 20 | PHF: 0.95 | SB | SBT SBR | 20 20 | 606 0 | 7 0 | 1% | 635 0 | 0 | 635 |
| | 20 | 0.95 | TEV | TEV | 20 | 2235 | 53 | 0% | 2350 | 0 | 0 2350 |
| | | | IEV | IEV | 20 | 2233 | | | 2550 | | 2330 |
| 3 | 30 | SW 2nd Ave @SW Jefferson St | Т | EBL | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | 2 hr PM Turning Movement Count | EB | EBT | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | Count Date: 2/26/2015 | | EBR | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | 2015 | | WBL | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | Signalized | WB | WBT | 30 | 372 | 7 | 2% | 390 | 0 | 390 |
| | 30 | DM D | | WBR | 30 | 258 | 0 | 0% | 270 | 0 | 270 |
| | 30 30 | PM Peak Hour: 4:30 PM-5:30 PM PM Peak Hour Used: 4:45 PM-5:45 PM | NB | NBL NBT | 30 30 | 113 376 | 2 | 2% 1% | 120 395 | 10 | 120 405 |
| | 30 | PM Peak Hour Used: 4.45 PM-5.45 PM | IND | NBR | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | | - | SBL | 30 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 30 | PHF: | SB | SBT | 30 | 0 | 0 | 0% | Ö | Ö | ů |
| | 30 | 0.95 | | SBR | 30 | 0 | Ō | 0% | 0 | 0 | Ō |
| | | | TEV | TEV | 30 | 1119 | 13 | | 1175 | 10 | 1185 |
| | 40 | OWA-LA COW I-ff OI | - | EBL | - 40 | 0 | 0 | 0% | 0 | 0 | |
| 4 | 40 | SW 1st Ave @SW Jefferson St 2 hr PM Turning Movement Count | EB | EBT | 40 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 40 | Count Date: 2/26/2015 | LD | EBR | 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 40 | 2015 | | WBL | 40 | 62 | 2 | 3% | 65 | Ö | 65 |
| | 40 | Signalized | WB | WBT | 40 | 209 | 5 | 2% | 220 | Ö | 220 |
| | 40 | | | WBR | 40 | 0 | Ō | 0% | 0 | 0 | 0 |
| 1 | 40 | PM Peak Hour: 4:30 PM-5:30 PM | | NBL | 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| 1 | 40 | PM Peak Hour Used: 4:45 PM-5:45 PM | NB | NBT | 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 40 | | | NBR | 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| 1 | 40 | BUE. | OD | SBL | 40 | 0 | 0 | 0% | 0 | 0 | 0 |
| 1 | 40 | PHF: | SB | SBT | 40 | 496 178 | 5 | 1% | 520 | 0 | 520 |
| | 40 | 0.86 0 | TEV | SBR TEV | 40 40 | 945 | 14 | 1% | 185 990 | 0 | 185 990 |
| | | | I IEV | I IEV | 40 | 340 | 14 | | 330 | | 330 |
| 5 | 50 | SW Naito Pkwy @SW Jefferson St | | EBL | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 50 | 2 hr PM Turning Movement Count | EB | EBT | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 50 | Count Date: 2/26/2015 | | EBR | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 50 | 2015 | | WBL | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 50 | Signalized | WB | WBT | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| 1 | 50 50 | DM Deals Have 4:00 DM 5:00 DM | | WBR | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| 1 | 50 50 | PM Peak Hour: 4:00 PM-5:00 PM PM Peak Hour Used: 4:45 PM-5:45 PM | NB | NBL NBT | 50 50 | 93 1025 | 8 13 | 9% 1% | 100 1075 | 0 | 100 1075 |
| 1 | 50 50 | I WIT GRA FIGUR USEG. 4.40 PW-3.40 PW | IND | NBR | 50 | 359 | 4 | 1% 1% | 375 | 0 | 375 |
| | 50 | | - | SBL | 50 | 0 | 0 | 0% | 0 | 0 | 0 |
| | 50 | PHF: | SB | SBT | 50 | 1259 | 7 | 1% | 1325 | Ö | 1325 |
| | 50 | 0.96 | | SBR | 50 | 128 | 1 | 1% | 135 | 0 | 135 |
| | | | TEV | TEV | 50 | 2864 | 33 | | 3010 | 0 | 3010 |

Growth Rate =

Project: Multnomah County Courthouse
Job #: MULT0000-0072

Job #: MDLT0000-00/2 Subject: PM Turning Movement Volumes Created: 3/2/2015

Existing Counts 2015 1-Hr Volume Existing 2015 Rev. Date: 3/6/2015 Heavy Vehicle Volume Balancing **Heavy Vehicle Unbalanced Volumes Balanced Volumes** N-S ID Synchro ID Intersection Direction Movement Int ID PM Peak Percentage PM Peak Adjustments PM Peak SW 2nd Ave @SW Columbia St ЕВ 60 60 60 2 hr PM Turning Movement Count FBT 60 60 535 3% 0% 560 10 570 Count Date: 2/26/2015 2015 60 60 0% 0% WB Signalized 60 WBT 60 60 NRI PM Peak Hour: 4:45 PM-5:45 PM NB PM Peak Hour Used: 4:45 PM-5:45 PM 60 60 365 380 60 NBT 346 1% 3% 15 60 60 0% 0% PHF: SB SBT 60 60 **60** 60 0.98 1085 1140 1165 SW 1st Ave @SW Columbia St 70 EBL 0% 70 70 70 2 hr PM Turning Movement Count Count Date: 2/26/2015 ΕB 70 70 70 470 175 470 175 FRT 446 2% 10% EBR 2015 Signalized WB WBT 70 70 0% 0% 70 70 70 70 PM Peak Hour: 4:45 PM-5:45 PM 70 70 0% 0% PM Peak Hour Used: 4:45 PM-5:45 PM NB NBT 70 70 70 SB 70 PHF: SBT 438 2% 460 460 70 TEV 1172 TEV 80 SW 2nd Ave @SW Clay St FBI 2 hr PM Turning Movement Count Count Date: 2/26/2015 2015 ΕB 80 0% 80 80 80 80 80 WBI 80 80 0% 2% 347 WB WBT 365 365 1% 0% WBR NBL 80 PM Peak Hour: 4:15 PM-5:15 PM NBT NBR 80 PM Peak Hour Used: 4:45 PM-5:45 PM NB 80 80 183 1% 190 80 80 0% 0% 80 80 SB PHF-SBT 0.93 80 **80** 0% 824 TEV TEV 860 875 SW 1st Ave @SW Clay St 2 hr PM Turning Movement Count EBL EBT 0% 0% 90 ЕВ 90 Count Date: 2/26/2015 EBF 90 90 90 2015 WRI WB WBT 90 362 90 90 90 WBR 90 PM Peak Hour: 4:45 PM-5:45 PM PM Peak Hour Used: 4:45 PM-5:45 PM NB NBT 90 90 NBR 90 90 90 90 SBI SB SBT 90 550 90 0.96 SBF 90 1017 TEV TEV 90 1065 SW 1st Ave @SW Market St 100 100 EB 830 100 2 hr PM Turning Movement Count EBT 1% 870 875 100 100 100 Count Date: 2/26/2015 2015 FRR 100 100 100 0% 0% WBL WB Signalized 100 100 100 100 100 100 PM Peak Hour: 4:45 PM-5:45 PM NBI PM Peak Hour Used: 4:45 PM-5:45 PM NB NBT 0% 100 100 100 0% 7% 0% NBR 100 100 100 204 372 215 390 215 385 SB SBT 100 100 100 0.94 0% TEV TEV 1783 24 1870 1870 SW Naito Pkwy @SW Market St 360 110 110 EBL EBT 110 110 341 473 1% 1% EB 2 hr PM Turning Movement Count Count Date: 2/26/2015 2015 495 110 110 110 Signalized WB WBT 110 0% 0% 0 PM Peak Hour: 4:00 PM-5:00 PM 0% 2% 110 110 0 521 PM Peak Hour Used: 4:45 PM-5:45 PM NB 550 550 110 NBT 110 110 SB 785 1% 110 PHF SBT 110 825 825 110 0.96 3126 TEV 3290 3290

Updated - 3/3/2015

APPENDIX C – Traffic Operations

| | ۶ | → | • | • | ← | • | • | † | <i>></i> | > | ţ | - ✓ |
|-----------------------------------|--------|----------|-------|------|------------|------------|---------|-------------|-------------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 41∱ | | | | | | ∱ 1> | | | | |
| Volume (vph) | 65 | 1325 | 0 | 0 | 0 | 0 | 0 | 435 | 245 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | 4.0 | | | | | | 4.0 | | | | |
| Lane Util. Factor | | 0.95 | | | | | | 0.95 | | | | |
| Frpb, ped/bikes | | 1.00 | | | | | | 0.90 | | | | |
| Flpb, ped/bikes | | 1.00 | | | | | | 1.00 | | | | |
| Frt | | 1.00 | | | | | | 0.95 | | | | |
| Flt Protected | | 1.00 | | | | | | 1.00 | | | | |
| Satd. Flow (prot) | | 2967 | | | | | | 2591 | | | | |
| Flt Permitted | | 1.00 | | | | | | 1.00 | | | | |
| Satd. Flow (perm) | | 2967 | | | | | | 2591 | | | | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 68 | 1395 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 458 | 258 | 0.00 | 0.00 | 0.00 |
| RTOR Reduction (vph) | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1456 | 0 | 0 | 0 | 0 | 0 | 684 | 0 | 0 | 0 | 0 |
| Confl. Peds. (#/hr) | 130 | 1400 | O . | · · | U | U | U | 004 | 247 | U | U | J |
| Confl. Bikes (#/hr) | 100 | | | | | | | | 29 | | | |
| Heavy Vehicles (%) | 7% | 3% | 0% | 0% | 0% | 0% | 0% | 1% | 1% | 0% | 0% | 0% |
| Turn Type | Perm | NA | 0 70 | 0 70 | 0 70 | 0 70 | 0 70 | NA | 1 /0 | 0 70 | 0 70 | 0 70 |
| Protected Phases | FeIIII | 4 | | | | | | 2 | | | | |
| Permitted Phases | 4 | 4 | | | | | | | | | | |
| Actuated Green, G (s) | 4 | 35.0 | | | | | | 17.0 | | | | |
| Effective Green, g (s) | | 35.0 | | | | | | 17.0 | | | | |
| Actuated g/C Ratio | | 0.58 | | | | | | 0.28 | | | | |
| Clearance Time (s) | | 4.0 | | | | | | 4.0 | | | | |
| | | | | | | | | 734 | | | | |
| Lane Grp Cap (vph) v/s Ratio Prot | | 1730 | | | | | | c0.26 | | | | |
| | | 0.40 | | | | | | CU.20 | | | | |
| v/s Ratio Perm | | 0.49 | | | | | | 0.02 | | | | |
| v/c Ratio | | 0.84 | | | | | | 0.93 | | | | |
| Uniform Delay, d1 | | 10.2 | | | | | | 20.9 | | | | |
| Progression Factor | | 1.00 | | | | | | 0.57 | | | | |
| Incremental Delay, d2 | | 5.1 | | | | | | 19.2 | | | | |
| Delay (s) | | 15.4 | | | | | | 31.2 | | | | |
| Level of Service | | B | | | 0.0 | | | C | | | 0.0 | |
| Approach LOC | | 15.4 | | | 0.0 | | | 31.2 | | | 0.0 | |
| Approach LOS | | В | | | Α | | | С | | | А | |
| Intersection Summary | | | | | | | | | _ | | | |
| HCM 2000 Control Delay | | | 20.6 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.87 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization | า | | 87.0% | IC | CU Level o | of Service | | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | € | + | • | 4 | † | <i>></i> | / | + | 1 |
|-------------------------------|------------|------------|-------|------|-------------|------------|---------|------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | † † | 7 | | | | | | | | ተተኩ | |
| Volume (vph) | 0 | 1490 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 635 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | 4.2 | 4.2 | | | | | | | | 4.5 | |
| Lane Util. Factor | | 0.95 | 1.00 | | | | | | | | 0.91 | |
| Frpb, ped/bikes | | 1.00 | 0.94 | | | | | | | | 1.00 | |
| Flpb, ped/bikes | | 1.00 | 1.00 | | | | | | | | 0.98 | |
| Frt | | 1.00 | 0.85 | | | | | | | | 1.00 | |
| Flt Protected | | 1.00 | 1.00 | | | | | | | | 0.99 | |
| Satd. Flow (prot) | | 2988 | 1296 | | | | | | | | 4232 | |
| Flt Permitted | | 1.00 | 1.00 | | | | | | | | 0.99 | |
| Satd. Flow (perm) | | 2988 | 1296 | | | | | | | | 4232 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1568 | 84 | 0 | 0 | 0 | 0 | 0 | 0 | 153 | 668 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 0 |
| Lane Group Flow (vph) | 0 | 1568 | 74 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 788 | 0 |
| Confl. Peds. (#/hr) | | | 103 | | | | | | | 91 | | |
| Heavy Vehicles (%) | 0% | 3% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 1% | 1% | 0% |
| Turn Type | | NA | Perm | | | | | | | Perm | NA | |
| Protected Phases | | 4 | | | | | | | | | 2 | |
| Permitted Phases | | | 4 | | | | | | | 2 | | |
| Actuated Green, G (s) | | 38.8 | 38.8 | | | | | | | | 12.5 | |
| Effective Green, g (s) | | 38.8 | 38.8 | | | | | | | | 12.5 | |
| Actuated g/C Ratio | | 0.65 | 0.65 | | | | | | | | 0.21 | |
| Clearance Time (s) | | 4.2 | 4.2 | | | | | | | | 4.5 | |
| Lane Grp Cap (vph) | | 1932 | 838 | | | | | | | | 881 | |
| v/s Ratio Prot | | c0.52 | | | | | | | | | | |
| v/s Ratio Perm | | | 0.06 | | | | | | | | 0.19 | |
| v/c Ratio | | 0.81 | 0.09 | | | | | | | | 0.89 | |
| Uniform Delay, d1 | | 7.9 | 4.0 | | | | | | | | 23.1 | |
| Progression Factor | | 0.30 | 0.29 | | | | | | | | 1.00 | |
| Incremental Delay, d2 | | 1.9 | 0.1 | | | | | | | | 13.5 | |
| Delay (s) | | 4.3 | 1.3 | | | | | | | | 36.6 | |
| Level of Service | | Α | Α | | | | | | | | D | |
| Approach Delay (s) | | 4.1 | | | 0.0 | | | 0.0 | | | 36.6 | |
| Approach LOS | | Α | | | Α | | | Α | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.9 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.83 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | | um of lost | | | | 8.7 | | | |
| Intersection Capacity Utiliza | tion | | 97.0% | IC | CU Level of | of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

c Critical Lane Group

| | ٠ | → | • | • | ← | 4 | 1 | † | <i>></i> | / | ţ | 1 |
|-----------------------------------|-------|----------|-------|------|-----------|------------|---------|-----------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | ^ | 7 | | 41∱ | | | | |
| Volume (vph) | 0 | 0 | 0 | 0 | 390 | 270 | 120 | 405 | 0 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | | | | 4.0 | 4.0 | | 4.0 | | | | |
| Lane Util. Factor | | | | | 0.95 | 1.00 | | 0.95 | | | | |
| Frpb, ped/bikes | | | | | 1.00 | 0.96 | | 1.00 | | | | |
| Flpb, ped/bikes | | | | | 1.00 | 1.00 | | 0.99 | | | | |
| Frt | | | | | 1.00 | 0.85 | | 1.00 | | | | |
| Flt Protected | | | | | 1.00 | 1.00 | | 0.99 | | | | |
| Satd. Flow (prot) | | | | | 3018 | 1327 | | 2967 | | | | |
| Flt Permitted | | | | | 1.00 | 1.00 | | 0.99 | | | | |
| Satd. Flow (perm) | | | | | 3018 | 1327 | | 2967 | | | | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 0 | 411 | 284 | 126 | 426 | 0 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 146 | 0 | 46 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 411 | 138 | 0 | 506 | 0 | 0 | 0 | 0 |
| Confl. Peds. (#/hr) | | | | | | 39 | 77 | | | | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 2% | 0% | 2% | 1% | 0% | 0% | 0% | 0% |
| Turn Type | | | | | NA | Perm | Perm | NA | | | | |
| Protected Phases | | | | | 4 | . 0 | . 0 | 2 | | | | |
| Permitted Phases | | | | | • | 4 | 2 | _ | | | | |
| Actuated Green, G (s) | | | | | 28.0 | 28.0 | _ | 24.0 | | | | |
| Effective Green, g (s) | | | | | 28.0 | 28.0 | | 24.0 | | | | |
| Actuated g/C Ratio | | | | | 0.47 | 0.47 | | 0.40 | | | | |
| Clearance Time (s) | | | | | 4.0 | 4.0 | | 4.0 | | | | |
| Lane Grp Cap (vph) | | | | | 1408 | 619 | | 1186 | | | | |
| v/s Ratio Prot | | | | | c0.14 | 010 | | 1100 | | | | |
| v/s Ratio Perm | | | | | 00.14 | 0.10 | | 0.17 | | | | |
| v/c Ratio | | | | | 0.29 | 0.10 | | 0.43 | | | | |
| Uniform Delay, d1 | | | | | 9.9 | 9.5 | | 13.0 | | | | |
| Progression Factor | | | | | 1.10 | 1.49 | | 0.76 | | | | |
| Incremental Delay, d2 | | | | | 0.5 | 0.8 | | 1.0 | | | | |
| Delay (s) | | | | | 11.4 | 15.0 | | 10.9 | | | | |
| Level of Service | | | | | В | 10.0 B | | 10.5 B | | | | |
| Approach Delay (s) | | 0.0 | | | 12.9 | | | 10.9 | | | 0.0 | |
| Approach LOS | | A | | | В | | | В | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 12.0 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.35 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | S | um of los | t time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | 1 | | 77.2% | | | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | • | ← | • | 4 | † | <i>></i> | / | ļ | 4 |
|----------------------------------|---------|----------|-------|------|------------|------------|---------|------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 4∱ | | | | | | ^ | 7 |
| Volume (vph) | 0 | 0 | 0 | 65 | 220 | 0 | 0 | 0 | 0 | 0 | 520 | 185 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | | | | 4.0 | | | | | | 4.0 | 4.0 |
| Lane Util. Factor | | | | | 0.95 | | | | | | 0.95 | 1.00 |
| Frpb, ped/bikes | | | | | 1.00 | | | | | | 1.00 | 0.88 |
| Flpb, ped/bikes | | | | | 0.99 | | | | | | 1.00 | 1.00 |
| Frt | | | | | 1.00 | | | | | | 1.00 | 0.85 |
| Flt Protected | | | | | 0.99 | | | | | | 1.00 | 1.00 |
| Satd. Flow (prot) | | | | | 2936 | | | | | | 3048 | 1194 |
| Flt Permitted | | | | | 0.99 | | | | | | 1.00 | 1.00 |
| Satd. Flow (perm) | | | | | 2936 | | | | | | 3048 | 1194 |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Adj. Flow (vph) | 0 | 0 | 0 | 76 | 256 | 0 | 0 | 0 | 0 | 0 | 605 | 215 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 111 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 286 | 0 | 0 | 0 | 0 | 0 | 605 | 104 |
| Confl. Peds. (#/hr) | | | | 76 | | | | | | | | 185 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 3% | 2% | 0% | 0% | 0% | 0% | 0% | 1% | 1% |
| Turn Type | | | | Perm | NA | | | | | | NA | Perm |
| Protected Phases | | | | | 4 | | | | | | 2 | |
| Permitted Phases | | | | 4 | | | | | | | | 2 |
| Actuated Green, G (s) | | | | | 23.0 | | | | | | 29.0 | 29.0 |
| Effective Green, g (s) | | | | | 23.0 | | | | | | 29.0 | 29.0 |
| Actuated g/C Ratio | | | | | 0.38 | | | | | | 0.48 | 0.48 |
| Clearance Time (s) | | | | | 4.0 | | | | | | 4.0 | 4.0 |
| Lane Grp Cap (vph) | | | | | 1125 | | | | | | 1473 | 577 |
| v/s Ratio Prot | | | | | | | | | | | c0.20 | |
| v/s Ratio Perm | | | | | 0.10 | | | | | | | 0.09 |
| v/c Ratio | | | | | 0.25 | | | | | | 0.41 | 0.18 |
| Uniform Delay, d1 | | | | | 12.6 | | | | | | 10.0 | 8.8 |
| Progression Factor | | | | | 1.00 | | | | | | 0.65 | 1.47 |
| Incremental Delay, d2 | | | | | 0.5 | | | | | | 0.6 | 0.4 |
| Delay (s) | | | | | 13.2 | | | | | | 7.1 | 13.3 |
| Level of Service | | | | | В | | | | | | Α | В |
| Approach Delay (s) | | 0.0 | | | 13.2 | | | 0.0 | | | 8.7 | |
| Approach LOS | | Α | | | В | | | Α | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 10.0 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capacity | y ratio | | 0.34 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | S | um of lost | time (s) | | | 8.0 | | | |
| Intersection Capacity Utilizatio | n | | 71.0% | IC | CU Level o | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ٠ | • | * | † | ↓ | 4 | |
|-------------------------------|------------|-------|------------|------------|------------|------------------|----------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | | | 7 | † † | † ‡ | 02.11 | |
| Volume (vph) | 0 | 0 | 100 | 1450 | 1325 | 135 | |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | |
| Total Lost time (s) | 1000 | 1000 | 4.0 | 4.5 | 4.5 | 1000 | |
| Lane Util. Factor | | | 1.00 | 0.95 | 0.95 | | |
| Frpb, ped/bikes | | | 1.00 | 1.00 | 1.00 | | |
| Flpb, ped/bikes | | | 1.00 | 1.00 | 1.00 | | |
| Frt | | | 1.00 | 1.00 | 0.99 | | |
| Flt Protected | | | 0.95 | 1.00 | 1.00 | | |
| Satd. Flow (prot) | | | 1563 | 3386 | 3325 | | |
| Flt Permitted | | | 0.17 | 1.00 | 1.00 | | |
| Satd. Flow (perm) | | | 279 | 3386 | 3325 | | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | |
| Adj. Flow (vph) | 0.50 | 0.50 | 104 | 1510 | 1380 | 141 | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 9 | 0 | |
| Lane Group Flow (vph) | 0 | 0 | 104 | 1510 | 1512 | 0 | |
| Confl. Peds. (#/hr) | | | 16 | 1010 | 1012 | 16 | |
| Confl. Bikes (#/hr) | | | 10 | | | 15 | |
| Heavy Vehicles (%) | 0% | 0% | 9% | 1% | 1% | 1% | |
| Turn Type | 0 70 | 0 / 0 | custom | NA | NA | . , , | |
| Protected Phases | | | Custom | 24 | 2 | | |
| Permitted Phases | | | 4 | ۷ ٦ | | | |
| Actuated Green, G (s) | | | 30.5 | 90.0 | 51.0 | | |
| Effective Green, g (s) | | | 30.5 | 86.0 | 51.0 | | |
| Actuated g/C Ratio | | | 0.34 | 0.96 | 0.57 | | |
| Clearance Time (s) | | | 4.0 | 0.00 | 4.5 | | |
| Vehicle Extension (s) | | | 1.0 | | 0.2 | | |
| Lane Grp Cap (vph) | | | 94 | 3235 | 1884 | | |
| v/s Ratio Prot | | | 34 | 0.45 | c0.45 | | |
| v/s Ratio Perm | | | c0.37 | 0.40 | 00.40 | | |
| v/c Ratio | | | 1.11 | 0.47 | 0.80 | | |
| Uniform Delay, d1 | | | 29.8 | 0.47 | 15.5 | | |
| Progression Factor | | | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | | | 124.5 | 0.0 | 3.7 | | |
| Delay (s) | | | 154.3 | 0.0 | 19.2 | | |
| Level of Service | | | 154.2 F | 0.2 A | 19.2 B | | |
| Approach Delay (s) | 0.0 | | | 10.1 | 19.2 | | |
| Approach LOS | 0.0 A | | | В | 19.2 B | | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 14.5 | Ц | CM 2000 | Level of Service | В |
| HCM 2000 Volume to Capa | city ratio | | 0.91 | - 11 | OIVI 2000 | LOVE OF OUR | U |
| Actuated Cycle Length (s) | only ratio | | 90.0 | Q | um of lost | time (s) | 8.5 |
| Intersection Capacity Utiliza | tion | | 51.4% | | CU Level o | | 0.5 A |
| Analysis Period (min) | iuOH | | 15 | ic | O FEASI O | 1 OEI VICE | ^ |
| c Critical Lane Group | | | 10 | | | | |
| onlical Lane Group | | | | | | | |

| | ۶ | → | • | • | + | • | 4 | † | <i>></i> | \ | + | 1 |
|-----------------------------------|-------|----------|-------|------|------------|------------|---------|-------------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 41₽ | | | | | | ↑ 1> | | | | |
| Volume (vph) | 140 | 570 | 0 | 0 | 0 | 0 | 0 | 380 | 75 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | 4.0 | | | | | | 4.0 | | | | |
| Lane Util. Factor | | 0.95 | | | | | | 0.95 | | | | |
| Frpb, ped/bikes | | 1.00 | | | | | | 0.98 | | | | |
| Flpb, ped/bikes | | 0.99 | | | | | | 1.00 | | | | |
| Frt | | 1.00 | | | | | | 0.98 | | | | |
| Flt Protected | | 0.99 | | | | | | 1.00 | | | | |
| Satd. Flow (prot) | | 2915 | | | | | | 2907 | | | | |
| Flt Permitted | | 0.99 | | | | | | 1.00 | | | | |
| Satd. Flow (perm) | | 2915 | | | | | | 2907 | | | | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 143 | 582 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 388 | 77 | 0.00 | 0.00 | 0.00 |
| RTOR Reduction (vph) | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 689 | 0 | 0 | 0 | 0 | 0 | 437 | 0 | 0 | 0 | 0 |
| Confl. Peds. (#/hr) | 117 | 003 | U | U | U | U | U | 701 | 116 | U | U | U |
| Confl. Bikes (#/hr) | 117 | | | | | | | | 33 | | | |
| Heavy Vehicles (%) | 3% | 3% | 0% | 0% | 0% | 0% | 0% | 1% | 3% | 0% | 0% | 0% |
| | | NA | 0 70 | 0 70 | 0 70 | 0 70 | 0 70 | NA | J /0 | 0 /0 | 0 70 | 0 70 |
| Turn Type Protected Phases | Perm | | | | | | | | | | | |
| | 4 | 4 | | | | | | 2 | | | | |
| Permitted Phases | 4 | 00.0 | | | | | | 04.0 | | | | |
| Actuated Green, G (s) | | 28.0 | | | | | | 24.0 | | | | |
| Effective Green, g (s) | | 28.0 | | | | | | 24.0 | | | | |
| Actuated g/C Ratio | | 0.47 | | | | | | 0.40 | | | | |
| Clearance Time (s) | | 4.0 | | | | | | 4.0 | | | | |
| Lane Grp Cap (vph) | | 1360 | | | | | | 1162 | | | | |
| v/s Ratio Prot | | | | | | | | c0.15 | | | | |
| v/s Ratio Perm | | 0.24 | | | | | | | | | | |
| v/c Ratio | | 0.51 | | | | | | 0.38 | | | | |
| Uniform Delay, d1 | | 11.2 | | | | | | 12.7 | | | | |
| Progression Factor | | 1.00 | | | | | | 1.40 | | | | |
| Incremental Delay, d2 | | 1.4 | | | | | | 0.9 | | | | |
| Delay (s) | | 12.5 | | | | | | 18.7 | | | | |
| Level of Service | | В | | | | | | В | | | | |
| Approach Delay (s) | | 12.5 | | | 0.0 | | | 18.7 | | | 0.0 | |
| Approach LOS | | В | | | Α | | | В | | | Α | |
| Intersection Summary | | | · | | | | | | | | | |
| HCM 2000 Control Delay | | | 14.9 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.45 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization |) | | 76.6% | IC | U Level of | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | • | + | • | 4 | † | <i>></i> | / | ţ | -√ |
|-----------------------------------|-------|-------------|-------|------|-------------|------------|---------|--|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ∱ 1> | | | | | | | | | 414 | |
| Volume (vph) | 0 | 470 | 175 | 0 | 0 | 0 | 0 | 0 | 0 | 130 | 460 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | 4.0 | | | | | | | | | 4.0 | |
| Lane Util. Factor | | 0.95 | | | | | | | | | 0.95 | |
| Frpb, ped/bikes | | 0.97 | | | | | | | | | 1.00 | |
| Flpb, ped/bikes | | 1.00 | | | | | | | | | 0.98 | |
| Frt | | 0.96 | | | | | | | | | 1.00 | |
| Flt Protected | | 1.00 | | | | | | | | | 0.99 | |
| Satd. Flow (prot) | | 2752 | | | | | | | | | 2926 | |
| FIt Permitted | | 1.00 | | | | | | | | | 0.99 | |
| Satd. Flow (perm) | | 2752 | | | | | | | | | 2926 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0.00 | 495 | 184 | 0 | 0 | 0 | 0 | 0 | 0 | 137 | 484 | 0.00 |
| RTOR Reduction (vph) | 0 | 64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 0 |
| Lane Group Flow (vph) | 0 | 615 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 578 | 0 |
| Confl. Peds. (#/hr) | J | 0.0 | 116 | | | • | • | , and the second | | 143 | 0.0 | |
| Confl. Bikes (#/hr) | | | 39 | | | | | | | 110 | | |
| Heavy Vehicles (%) | 0% | 2% | 10% | 0% | 0% | 0% | 0% | 0% | 0% | 1% | 2% | 0% |
| Turn Type | 0 70 | NA | 1070 | 0 70 | 0 70 | 070 | 070 | 070 | 070 | Perm | NA | 0 70 |
| Protected Phases | | 4 | | | | | | | | I CIIII | 2 | |
| Permitted Phases | | | | | | | | | | 2 | | |
| Actuated Green, G (s) | | 26.0 | | | | | | | | 2 | 26.0 | |
| Effective Green, g (s) | | 26.0 | | | | | | | | | 26.0 | |
| Actuated g/C Ratio | | 0.43 | | | | | | | | | 0.43 | |
| Clearance Time (s) | | 4.0 | | | | | | | | | 4.0 | |
| Lane Grp Cap (vph) | | 1192 | | | | | | | | | 1267 | |
| v/s Ratio Prot | | c0.22 | | | | | | | | | 1207 | |
| v/s Ratio Perm | | 60.22 | | | | | | | | | 0.20 | |
| v/c Ratio | | 0.52 | | | | | | | | | 0.46 | |
| Uniform Delay, d1 | | 12.4 | | | | | | | | | 12.0 | |
| Progression Factor | | 0.31 | | | | | | | | | 0.73 | |
| Incremental Delay, d2 | | 1.4 | | | | | | | | | 1.1 | |
| Delay (s) | | 5.3 | | | | | | | | | 9.8 | |
| Level of Service | | 3.3 A | | | | | | | | | 9.0 A | |
| Approach Delay (s) | | 5.3 | | | 0.0 | | | 0.0 | | | 9.8 | |
| Approach LOS | | 3.5 A | | | Α | | | Α | | | 9.0 A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 7.5 | Н | CM 2000 | Level of S | Service | | Α | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.49 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 76.0% | IC | CU Level of | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | • | ← | • | 4 | † | / | > | ţ | 4 |
|-----------------------------------|------|----------|-------|------|------------|------------|------|----------|----------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | ∱ ∱ | | Ŋ | † | | | | |
| Volume (veh/h) | 0 | 0 | 0 | 0 | 365 | 255 | 65 | 190 | 0 | 0 | 0 | 0 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Hourly flow rate (vph) | 0 | 0 | 0 | 0 | 392 | 274 | 70 | 204 | 0 | 0 | 0 | 0 |
| Pedestrians | | 98 | | | | | | | | | 57 | |
| Lane Width (ft) | | 0.0 | | | | | | | | | 0.0 | |
| Walking Speed (ft/s) | | 4.0 | | | | | | | | | 4.0 | |
| Percent Blockage | | 0 | | | | | | | | | 0 | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | 272 | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 724 | | | 0 | | | 294 | 724 | 0 | 689 | 587 | 488 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 724 | | | 0 | | | 294 | 724 | 0 | 689 | 587 | 488 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 100 | | | 89 | 42 | 100 | 100 | 100 | 100 |
| cM capacity (veh/h) | 888 | | | 1636 | | | 641 | 353 | 1091 | 181 | 425 | 531 |
| Direction, Lane # | WB 1 | WB 2 | NB 1 | NB 2 | | | | | | | | |
| Volume Total | 262 | 405 | 70 | 204 | | | | | | | | |
| Volume Left | 0 | 0 | 70 | 0 | | | | | | | | |
| Volume Right | 0 | 274 | 0 | 0 | | | | | | | | |
| cSH | 1700 | 1700 | 641 | 353 | | | | | | | | |
| Volume to Capacity | 0.15 | 0.24 | 0.11 | 0.58 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0.21 | 9 | 87 | | | | | | | | |
| Control Delay (s) | 0.0 | 0.0 | 11.3 | 28.4 | | | | | | | | |
| Lane LOS | 0.0 | 0.0 | В | D | | | | | | | | |
| Approach Delay (s) | 0.0 | | 24.0 | | | | | | | | | |
| Approach LOS | 0.0 | | С | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.0 | | | | | | | | | |
| Intersection Capacity Utilization | n | | 50.5% | IC | CU Level c | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

| | ۶ | → | • | • | + | • | 1 | † | <i>></i> | / | ţ | 1 |
|-----------------------------------|-------|----------|-------|---------|------------|------------|---------|------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | | | | 41 | | | | | | ተ ኈ | |
| Volume (vph) | 0 | 0 | 0 | 50 | 380 | 0 | 0 | 0 | 0 | 0 | 550 | 90 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | | | | 4.0 | | | | | | 4.0 | |
| Lane Util. Factor | | | | | 0.95 | | | | | | 0.95 | |
| Frpb, ped/bikes | | | | | 1.00 | | | | | | 0.98 | |
| Flpb, ped/bikes | | | | | 0.99 | | | | | | 1.00 | |
| Frt | | | | | 1.00 | | | | | | 0.98 | |
| Flt Protected | | | | | 0.99 | | | | | | 1.00 | |
| Satd. Flow (prot) | | | | | 2963 | | | | | | 2865 | |
| Flt Permitted | | | | | 0.99 | | | | | | 1.00 | |
| Satd. Flow (perm) | | | | | 2963 | | | | | | 2865 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 0.00 | 0.00 | 0 | 52 | 396 | 0 | 0 | 0 | 0 | 0 | 573 | 94 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 22 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 431 | 0 | 0 | 0 | 0 | 0 | 645 | 0 |
| Confl. Peds. (#/hr) | · · | • | · · | 105 | 101 | · · | | · · | V | • | 010 | 143 |
| Confl. Bikes (#/hr) | | | | 100 | | | | | | | | 16 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 5% | 2% | 0% | 0% | 0% | 0% | 0% | 3% | 7% |
| Turn Type | 0 70 | 0 70 | 070 | Perm | NA | 0 70 | 0 70 | 0 70 | 0 70 | 070 | NA | 1 70 |
| Protected Phases | | | | i Giiii | 4 | | | | | | 2 | |
| Permitted Phases | | | | 4 | | | | | | | | |
| Actuated Green, G (s) | | | | - | 24.0 | | | | | | 28.0 | |
| Effective Green, g (s) | | | | | 24.0 | | | | | | 28.0 | |
| Actuated g/C Ratio | | | | | 0.40 | | | | | | 0.47 | |
| Clearance Time (s) | | | | | 4.0 | | | | | | 4.0 | |
| Lane Grp Cap (vph) | | | | | 1185 | | | | | | 1337 | |
| v/s Ratio Prot | | | | | 1105 | | | | | | c0.23 | |
| v/s Ratio Perm | | | | | 0.15 | | | | | | 60.23 | |
| v/c Ratio | | | | | 0.15 | | | | | | 0.48 | |
| Uniform Delay, d1 | | | | | 12.6 | | | | | | 11.0 | |
| Progression Factor | | | | | 1.00 | | | | | | 0.91 | |
| | | | | | 0.9 | | | | | | 1.1 | |
| Incremental Delay, d2 | | | | | 13.5 | | | | | | 11.2 | |
| Delay (s) Level of Service | | | | | | | | | | | | |
| | | 0.0 | | | B 13.5 | | | 0.0 | | | B 11.2 | |
| Approach Delay (s) Approach LOS | | Α | | | 13.5 B | | | Α | | | 11.2 B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 12.1 | H | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | S | um of lost | time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 78.3% | | | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | • | + | • | • | † | <i>></i> | / | ↓ | -√ |
|-----------------------------------|-------|-------------|-------|------|-------------|------------|---------|------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4111 | | | | | | | | ሻሻ | † | |
| Volume (vph) | 0 | 875 | 395 | 0 | 0 | 0 | 0 | 0 | 0 | 215 | 385 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | | 5.4 | | | | | | | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.86 | | | | | | | | 0.97 | 1.00 | |
| Frpb, ped/bikes | | 0.97 | | | | | | | | 1.00 | 1.00 | |
| Flpb, ped/bikes | | 1.00 | | | | | | | | 0.94 | 1.00 | |
| Frt | | 0.95 | | | | | | | | 1.00 | 1.00 | |
| Flt Protected | | 1.00 | | | | | | | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 5132 | | | | | | | | 2625 | 1604 | |
| Flt Permitted | | 1.00 | | | | | | | | 0.95 | 1.00 | |
| Satd. Flow (perm) | | 5132 | | | | | | | | 2625 | 1604 | |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 0.01 | 931 | 420 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 229 | 410 | 0.01 |
| RTOR Reduction (vph) | 0 | 136 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1215 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 186 | 410 | 0 |
| Confl. Peds. (#/hr) | U | 1210 | 34 | · · | U | U | J | U | U | 90 | 710 | J |
| Confl. Bikes (#/hr) | | | 26 | | | | | | | 30 | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 7% | 1% | 0% |
| Turn Type | 0 70 | NA | 0 70 | 0 70 | 0 70 | 0 70 | 0 70 | 0 70 | 0 70 | Perm | NA | 0 70 |
| Protected Phases | | 4 | | | | | | | | Fellii | 2 | |
| Permitted Phases | | 4 | | | | | | | | 2 | | |
| Actuated Green, G (s) | | 22.8 | | | | | | | | 27.3 | 27.3 | |
| Effective Green, g (s) | | 22.8 | | | | | | | | 27.3 | 27.3 | |
| Actuated g/C Ratio | | 0.38 | | | | | | | | 0.46 | 0.46 | |
| Clearance Time (s) | | 5.4 | | | | | | | | 4.5 | 4.5 | |
| | | 1950 | | | | | | | | | 729 | |
| Lane Grp Cap (vph) | | | | | | | | | | 1194 | | |
| v/s Ratio Prot v/s Ratio Perm | | c0.24 | | | | | | | | 0.07 | c0.26 | |
| | | 0.60 | | | | | | | | 0.07 | 0.50 | |
| v/c Ratio | | 0.62 | | | | | | | | 0.16 | 0.56 | |
| Uniform Delay, d1 | | 15.1 | | | | | | | | 9.6 | 12.0 | |
| Progression Factor | | 1.00 | | | | | | | | 0.06 | 0.38 | |
| Incremental Delay, d2 | | 1.5 | | | | | | | | 0.3 | 2.8 | |
| Delay (s) | | 16.6 | | | | | | | | 8.0 | 7.4 | |
| Level of Service | | В | | | 0.0 | | | 0.0 | | Α | A | |
| Approach Delay (s) | | 16.6 | | | 0.0 | | | 0.0 | | | 5.0 | |
| Approach LOS | | В | | | Α | | | Α | | | Α | |
| Intersection Summary | | | | | | | | | _ | | | |
| HCM 2000 Control Delay | | | 12.9 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capacity | ratio | | 0.59 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.0 | | um of lost | | | | 9.9 | | | |
| Intersection Capacity Utilization | | | 78.3% | IC | CU Level of | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ۶ | → | • | • | + | • | 1 | † | <i>></i> | / | | 1 |
|-------------------------------|------------|----------|-------|------|------------|------------|---------|-------|-------------|----------|--------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | 4₽ | 7 | | | | | ተተኈ | | 1/4 | † † | |
| Volume (vph) | 360 | 495 | 235 | 0 | 0 | 0 | 0 | 550 | 15 | 810 | 825 | 0 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Total Lost time (s) | 4.9 | 4.9 | 4.9 | | | | | 4.5 | | 4.5 | 4.5 | |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | | | | | 0.91 | | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | | | | | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 0.97 | 1.00 | 1.00 | | | | | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | | | | | 1.00 | | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 0.99 | 1.00 | | | | | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1501 | 3209 | 1415 | | | | | 4786 | | 3285 | 3386 | |
| Flt Permitted | 0.95 | 0.99 | 1.00 | | | | | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1501 | 3209 | 1415 | | | | | 4786 | | 3285 | 3386 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 375 | 516 | 245 | 0 | 0 | 0 | 0 | 573 | 16 | 844 | 859 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 155 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 289 | 602 | 90 | 0 | 0 | 0 | 0 | 586 | 0 | 844 | 859 | 0 |
| Confl. Peds. (#/hr) | 20 | | 21 | | | | | | 35 | 35 | | |
| Confl. Bikes (#/hr) | | | | | | | | | 18 | | | |
| Heavy Vehicles (%) | 1% | 1% | 4% | 0% | 0% | 0% | 0% | 2% | 0% | 1% | 1% | 0% |
| Turn Type | Perm | NA | Perm | | | | | NA | | Prot | NA | |
| Protected Phases | | 4 | | | | | | 6 | | 5 | 2 | |
| Permitted Phases | 4 | | 4 | | | | | | | | | |
| Actuated Green, G (s) | 20.4 | 20.4 | 20.4 | | | | | 14.0 | | 41.7 | 60.2 | |
| Effective Green, g (s) | 20.4 | 20.4 | 20.4 | | | | | 14.0 | | 41.7 | 60.2 | |
| Actuated g/C Ratio | 0.23 | 0.23 | 0.23 | | | | | 0.16 | | 0.46 | 0.67 | |
| Clearance Time (s) | 4.9 | 4.9 | 4.9 | | | | | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 1.5 | 1.5 | 1.5 | | | | | 2.5 | | 0.2 | 0.2 | |
| Lane Grp Cap (vph) | 340 | 727 | 320 | | | | | 744 | | 1522 | 2264 | |
| v/s Ratio Prot | | | | | | | | c0.12 | | c0.26 | 0.25 | |
| v/s Ratio Perm | c0.19 | 0.19 | 0.06 | | | | | | | | | |
| v/c Ratio | 0.85 | 0.83 | 0.28 | | | | | 0.79 | | 0.55 | 0.38 | |
| Uniform Delay, d1 | 33.3 | 33.1 | 28.8 | | | | | 36.6 | | 17.4 | 6.6 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | | | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 17.1 | 7.4 | 0.2 | | | | | 5.3 | | 1.5 | 0.5 | |
| Delay (s) | 50.4 | 40.5 | 28.9 | | | | | 41.9 | | 18.9 | 7.1 | |
| Level of Service | D | D | С | | | | | D | | В | Α | |
| Approach Delay (s) | | 40.5 | | | 0.0 | | | 41.9 | | | 12.9 | |
| Approach LOS | | D | | | Α | | | D | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 27.1 | H | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.68 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | Sı | um of lost | time (s) | | | 13.9 | | | |
| Intersection Capacity Utiliza | ation | | 88.0% | | | of Service | | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group